

Superelevation Design Guide



**Engineering Division
Production Support**

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Part 1: Superelevation Quick Guide

Roadway Design Guidelines

Details on Superelevation design can be found in [Roadway Design Guidelines, Chapter 2-101.01](#)

Standard Roadway Drawings

- [RD11-SE-1](#)
- [RD11-SE-2](#)
- [RD11-SE-2A](#)
- [RD11-SE-3](#)
- [RD11-SE-3A](#)

TDOT Roadway Design Training Classes

- [GEOPAK Road Course Guide](#)
 - o Exercise 13: How to use MicroStation and GEOPAK to set up superelevation controlled shapes
 - o Exercise 14: How to apply the superelevation shapes to the cross sections
 - o Exercise 22: How to apply the superelevation shapes to the creation of the final TIN process.
- [Roadway Design Manual](#)
 - o Chapter 8: How to create the superelevation shapes and applying it to cross sections

TDOT Roadway Design Reference Documents

- [Plan-in-Hand Checklist](#)
- [PS&E Checklist](#)

Roadway Design Plans

In a standard roadway plan set, superelevation is included on the following sheets:

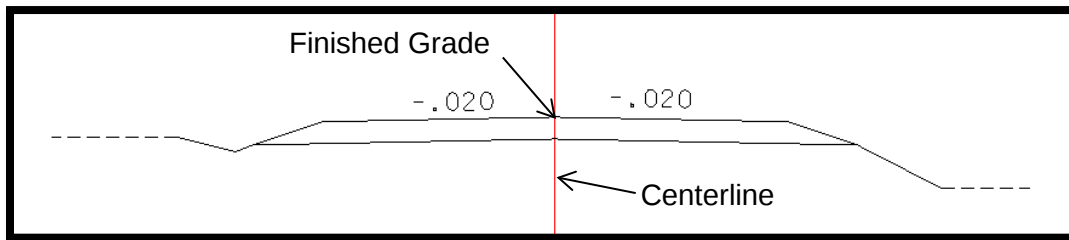
- Typical Sections Sheet: If a project has superelevation, a typical section and the station ranges of superelevation must be shown on this sheet.
- Proposed Profile: A superelevation diagram must be added to the Proposed Profile sheet.
- Cross Sections: The superelevation should be seen on the cross sections where superelevation is present.

Other Helpful Material

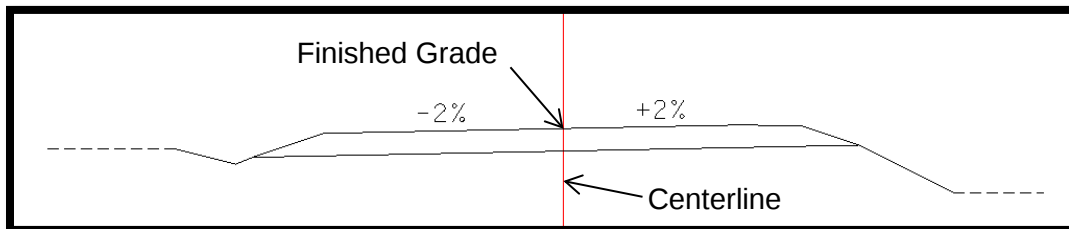
- Green Book (2011)

Part 2: Superelevation Calculation Guide

Superelevation is defined as the rate of cross slope on a curved section of roadway in which the outer edge is banked higher than the inner edge. The [Standard Roadway Drawings](#) provide information for Urban and Rural Superelevation Transition Details (RD11-SE-1 to RD11-SE-3A). Within the drawings, there are illustrations for a 2 lane and 4 or 6 lane road transition in superelevation. The following documentation will explain the log file created by running Superelevation in Geopak Road. It will also explain how to check information in the log file by performing calculations to find the stations where the lanes on each side of the centerline are at normal crown (-0.02) and where one of the lanes has transitioned from normal crown (-0.02) to straight surface or reverse crown (+0.02). Calculations will also be shown for the lane where maximum transition occurs from normal crown to a positive cross slope to identify the station where zero percent slope occurs.



Normal Crown



Reverse crown

The curve information that will be used for this example is for a rural 2 lane road based on the "E MAX = 0.08 Desirable" table on Standard Roadway Drawing RD11-SE-1 with $v = 30$ mph., degree of curve $13^{\circ}-00'$, maximum superelevation of 0.068, and transition length of 160.00'. When a horizontal alignment is added in Geopak Road, information for the curve can be found in Geopak Road by opening Coordinate Geometry>Navigator>Chain. Also, when the proposed horizontal alignment is displayed in the alignment file, the curve data will be part of the display. The curve data matches what is found in the Standard Roadway Drawing for Superelevation. The horizontal alignment and curve data are shown in *Figure 1- Horizontal Alignment Curve D1*. The SE, design speed, and transition length are all filled in by the user from the data in the standard drawing.

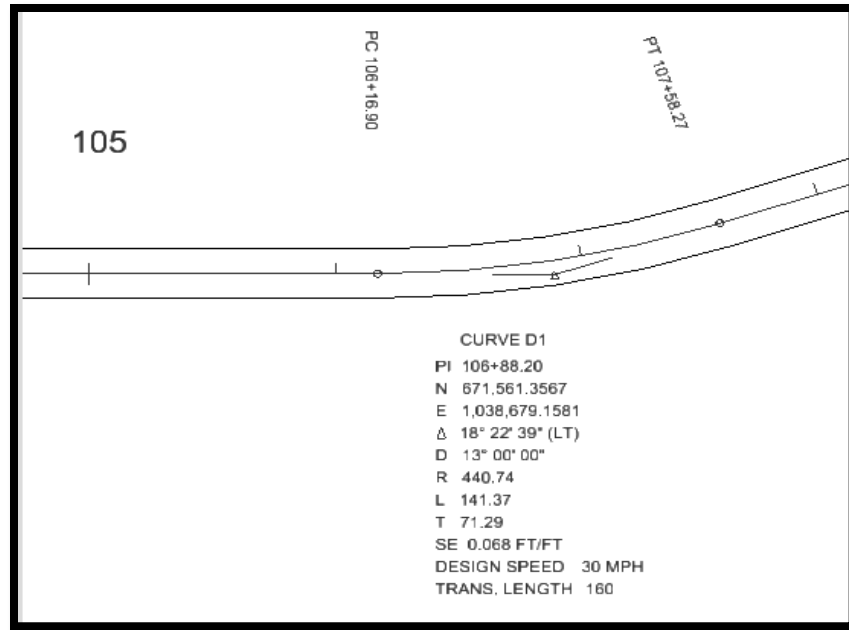


FIGURE 1 – HORIZONTAL ALIGNMENT CURVE D1

Notice the P.I. of the curve is to the right of the radius and the way the curve is laid out in *Figure 1- Horizontal Alignment Curve D1*. The transition from normal crown to full superelevation will begin on the right lane of the centerline first because that side goes from negative to positive cross slope while the other side remains negative.

The superelevation log file from Geopak Road contains information for the left and right lanes of the road as shown below. Because the transition begins on the right lane of the road, the right lane is listed first in the log file.

Left

ROADNAME 8.0000

filler line station / slope

100+00.000000 -2.0000

106+00.315956 -2.0000

106+87.588683 -6.8000 /* Curve D1 */

107+74.861410 -2.0000

112+03.385413 -2.0000

Right

ROADNAME -8.0000

filler line station / slope

100+00.000000 -2.0000

105+27.588683 -2.0000

106+87.588683 6.8000 /* Curve D1 */

108+47.588683 -2.0000

112+03.390000 -2.0000

The first entry line lists the road name and maximum superelevation rate from the “E MAX = 0.08 Desirable” table. The beginning and ending stations on the proposed horizontal alignment will

always be listed for both the left and right lanes of the road. For this alignment, the beginning and ending stations are 100+00.00 and 112+03.39. The output shows that full super occurs at station. 106+87.588683. The curve is only in full super for this station. This is because this station is at the midpoint of the curve** and begins to transition back down to normal crown. If the curve remained in full superelevation for more than a station, there would be an additional entry. For example, if the curve was in full superelevation for 100', there would be an additional entry of 107+87.588683 6.8000 /* Curve D1 */ , and the remaining stations would adjust accordingly.

Compare the output for the last station with normal crown listed on the right lane of the road (105+27.588683) prior to the full superelevation station with the last station with normal crown listed on the left lane of the of the road (106+00.315956). The station on the right precedes the station on the left because it has a longer transition. The same occurs after the full superelevation station where the station on the right (108+47.588683) follows the station of the left (107+74.861410) due to the longer transition length needed.

** In Figure 1, the length of the curve is shown to be 141.37.

$$141.37/2 = 70.69.$$

$$10616.90 \text{ (P.C.Sta.)} + 70.69 = 10687.59 = \text{Station } 106+87.59$$

This station (106+87.59) is the point on the curve with full superelevation.

The log file carries the numbers out 6 decimal places, but for the figures and calculations, only 2 decimal places will be used. When performing the calculations, there might be a slight difference in the 3rd decimal place due to rounding. Also, within the calculations, the plus sign in stations will be removed for clarity but will be shown in each result.

Verification and calculations for superelevation station:

For this example, the length of transition (160' from RD01-SE-3) is longer than the length of curve (141.37' from Geopak). Generally, one-half the transition length is before the PC and the other one-half is after the PC where maximum superelevation begins. Maximum superelevation continues to one-half the transition length before the PT and ends one-half the transition length after the PT. When the

Verification and calculations for stations will be shown for the right lane first:

Right

ROADNAME -8.0000

filler line station / slope

100+00.000000 -2.0000

105+27.588683 -2.0000

106+87.588683 6.8000 /* Curve D1 */

108+47.588683 -2.0000

112+03.390000 -2.0000

NORMAL CROWN BEFORE FULL SUPERELEVATION (RIGHT LANE)

To verify the last station where the right lane is at normal crown before it starts transitioning to full superelevation, subtract the transition length from the full superelevation station.

- Station of full Superelevation - Transition Length

$$10687.5887 - 160 = 105+27.5887$$

TRANSITION RATE

The transition rate for a curve is found for the lane of the road with the most change in cross slope, the right lane in this example. To find the transition rate, the maximum change in cross slope is divided by the known transition length for the curve.

- Transition Rate = $\frac{\text{Maximum Change in Cross Slope}}{\text{Known Transition Length of Curve}}$
$$= \frac{(0.068 - (-0.02))}{160'} = \frac{0.088}{160'} = 0.00055$$

This Transition Rate will be used in other calculations.

ZERO PERCENT BEFORE FULL SUPERELEVATION (RIGHT LANE)

Since the right lane of the road goes from a negative slope (normal crown slope of -0.02) to a positive slope at full super (+0.068), there is a station where the cross slope for the right lane is at zero percent (0.00). This is an area of concern because of drainage issues and should be analyzed by the designer to ensure no ponding occurs.

To find the station where zero percent cross slope occurs for the right lane of the road before reaching full superelevation, reverse the formula used to calculate the transition rate. Using the known transition rate and the change in cross slope, find the length needed to transition from normal crown cross slope to zero percent cross slope. Add the length to the last station where normal crown occurred.

- Length = $\frac{\text{Change in Cross Slope}}{\text{Transition Rate}}$
$$= \frac{0.00 - (-0.02)}{0.00055} = \frac{0.020}{0.00055} = 36.36'$$

Zero percent cross slope is reached at **10527.5887** + 36.36' = **105+63.95**

Another way to perform the calculation would have been to find the length of transition from zero percent cross slope to full superelevation cross slope and subtract from the superelevation station

- Length = $\frac{\text{Change in Cross Slope}}{\text{Transition Rate}}$
$$= \frac{(0.068 - 0.00)}{0.00055} = \frac{0.068}{0.00055} = 123.64'$$

Zero percent cross slope is reached at **10687.5887** – 123.64' = **105+63.95**

REVERSE CROWN BEFORE FULL SUPERELEVATION (RIGHT LANE)

To find the station where reverse crown (+0.02) occurs for the right lane of the road before reaching full superelevation, use the same calculations as previously described. Find the length needed to transition from normal crown cross slope to reverse crown and add the length to the last station where normal crown occurred.

- Length = $\frac{\text{Change in Cross Slope}}{\text{Transition Rate}}$
$$= \frac{0.02 - (-0.02)}{0.00055} = \frac{0.040}{0.00055} = 72.72'$$

OR

Double the number found in calculation #4 since it was calculated for a 0.02 change in cross slope, and this is a 0.04 change. $(36.36' \times 2) = 72.72'$

Reverse crown cross slope is reached at $10527.5887 + 72.72' = \underline{106+00.32}$

This station matches the station shown in the log file for the left lane of the road at the last station where normal crown occurs.

Once the right lane transitions from -0.20 to +0.20, both lanes will rotate at the same rate until full superelevation of 0.068 is reached (+0.068 for the right and -0.068 for the left).

FULL SUPERELEVATION

To verify the station where full superelevation is reached divide the curve length in half and add the result to the P.C. station.

P.C. Station + Curve Length / 2 =

$$10616.90 + (141.37/2) = \underline{106+87.59}$$

Since the curve is only at full superelevation for one station, the station can also be checked by using the P.T. station. To verify the station superelevation is reached, divide the curve length in half and subtract the result from the P.T. station.

P.T. Station – Curve Length/2 =

$$10758.27 - (141.37/2) = \underline{106+87.59}$$

REVERSE CROWN AFTER FULL SUPERELEVATION (RIGHT LANE)

To find the station where reverse crown (+0.02) occurs for the right lane of the road after full superelevation, use the same concept as previously described except use the station listed after the full superelevation where the cross slope has transitioned back to normal crown and subtract the calculated length (72.72') for a 0.04 change in cross slope.

Reverse crown cross slope is reached at $10847.5887 - 72.72' = \underline{107+74.86}$

This station matches the number shown in the log file for the left lane of the road for the last station where the left lane is at normal crown.

ZERO PERCENT AFTER FULL SUPERELEVATION (RIGHT LANE)

To find the station where zero percent cross slope occurs for the right lane of the road after reaching full superelevation, use the same concept as previously described except use the station after the superelevation where the cross slope has transitioned back to normal crown. Subtract the calculated length (36.36) for a 0.02 change in cross slope

Zero percent cross slope is reached at $10847.5887 - 36.36' = \underline{\underline{108+11.23}}$

Check: Full superelevation station plus length found for change from 0.00 to 0.068.

$$10687.5887 + 123.64' = \underline{\underline{108+11.23}}$$

NORMAL CROWN AFTER SUPERELEVATION (RIGHT LANE)

To verify where the right lane transitions back to normal crown after full superelevation is reached, add the transition length to the full superelevation station.

- Full Super + Transition Length

$$10687.5887 + 160 = \underline{\underline{108+47.5887}}$$

The next few steps will verify stations that are generated for the left lane of the road. The left lane of the road transitions from -0.02 to -0.068 so there is not a station for zero percent cross slope or reverse crown.

Left

ROADNAME 8.0000

filler line station / slope

100+00.000000 -2.0000

106+00.315956 -2.0000

106+87.588683 -6.8000 /* Curve D1 */

107+74.861410 -2.0000

112+03.385413 -2.0000

NORMAL CROWN BEFORE FULL SUPERELEVATION (LEFT LANE)

The full transition length of 160' is not needed on the left lane. The transition rate that was calculated for the right lane will be used to find the transition length needed to normal crown to superelevation. To verify the last station for normal crown prior to superelevation for the left lane, find the length needed for the change in cross slope from normal crown to full superelevation and divide by the known transition rate for the right lane. Subtract this length from the full superelevation station.

- Length = $\frac{\text{Change in Cross Slope}}{\text{Transition Rate}}$

$$= \frac{-0.068 - (-0.02)}{.00055} = \frac{0.048}{.00055} = 87.27$$

Full Super minus Length

$$10687.5887 - 87.27 = 106+00.32$$

This station matches the station calculated for reverse crown for the right lane.

NORMAL CROWN AFTER FULL SUPERELEVATION (LEFT LANE)

To find the station where the left lane transitions back to normal crown, add the length calculated for the left lane to the full superelevation station.

- Full Super + Length

$$10687.5887 + 87.27 = \underline{107+74.86}$$

This station matches the station calculated for reverse crown for the right lane.

Below is a figure for the entire curve with all the stations and cross slopes.

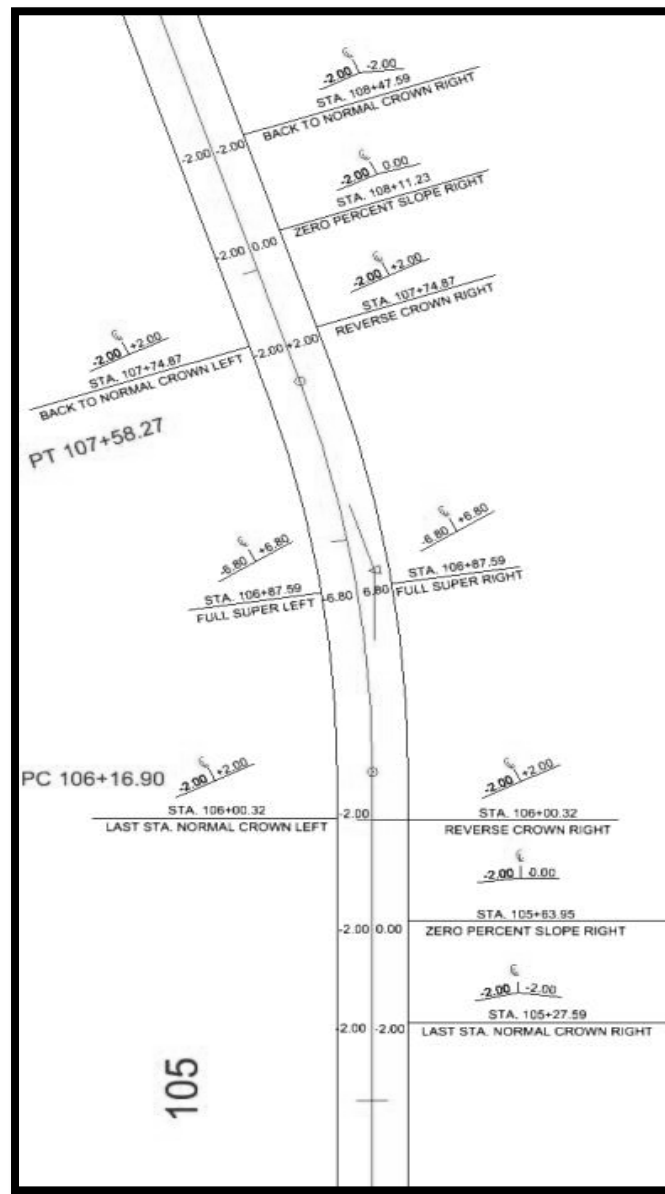


FIGURE 2 – STATIONS AND CROSS SLOPES

For clarity, the *Figure 2, Stations and Cross Slopes* has been split into two separate figures representing the stations before and after full superelevation.

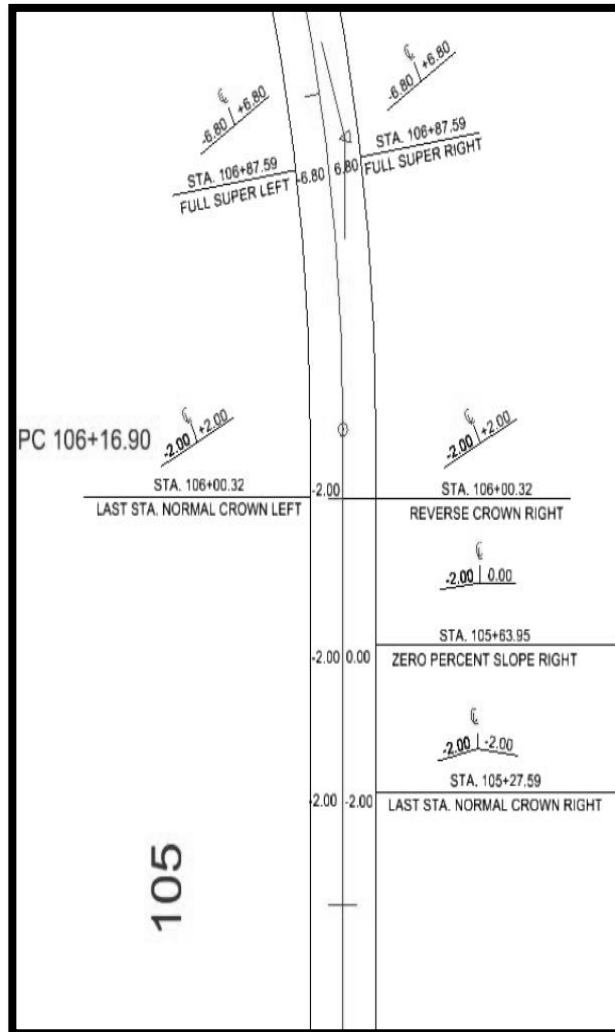


FIGURE 3 – STATIONS AND CROSS SLOPES BEFORE FULL SUPERELEVATION

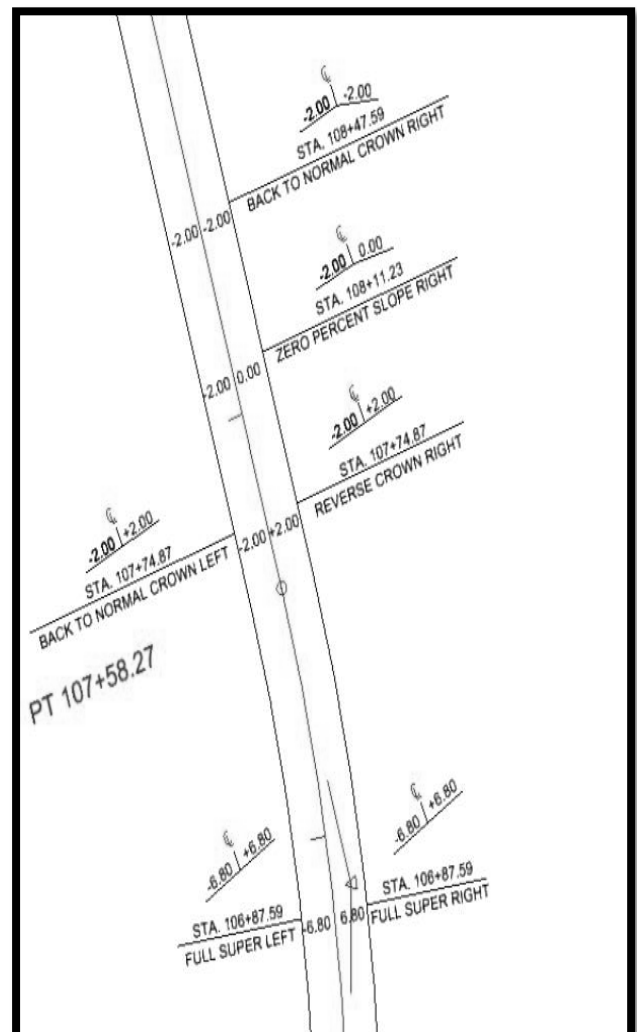


FIGURE 4 – STATIONS AND CROSS SLOPES AFTER FULL SUPERELEVATION

Part 3: Superelevation Calculation (RD11 Series)

Horizontal curves will no longer be identified by degree, they will be identified by radius only. Standard Drawings RD11-LR-1 (Urban) and RD11-LR-2 (Rural) contain tables for different design speeds, and number of lanes, showing the superelevation rate (e_d) associated with curve radius. One important thing to note that is different from the earlier standards is that for a specific e_d , the radius shown is the minimum radius that can be used. Also, for a given radius, only use the corresponding e_d .

③	e d (%)	V = 20 (MPH)					R MIN. (FT.)	
		R MIN. (FT.)	Number of lanes					
			2	3	4	5		6
	NC	1640	0	0	0	0	0	237
	2	1190	32	40	49	57	65	172
	2.2	1070	36	44	54	62	72	155
	2.4	959	39	48	58	68	78	140
	2.6	872	42	52	63	74	85	128
	2.8	796	45	57	68	79	91	117
	3	730	49	61	73	85	98	107
	3.2	672	52	65	78	91	104	98
	3.4	620	55	69	83	96	111	91
	3.6	572	58	73	88	102	117	84
	3.8	530	62	77	92	108	124	78
	4	490	65	81	97	114	130	72
	4.2	453	68	85	102	119	137	67
	4.4	418	71	89	107	125	143	63
	4.6	384	75	93	112	131	150	58
	4.8	349	78	97	117	136	156	54

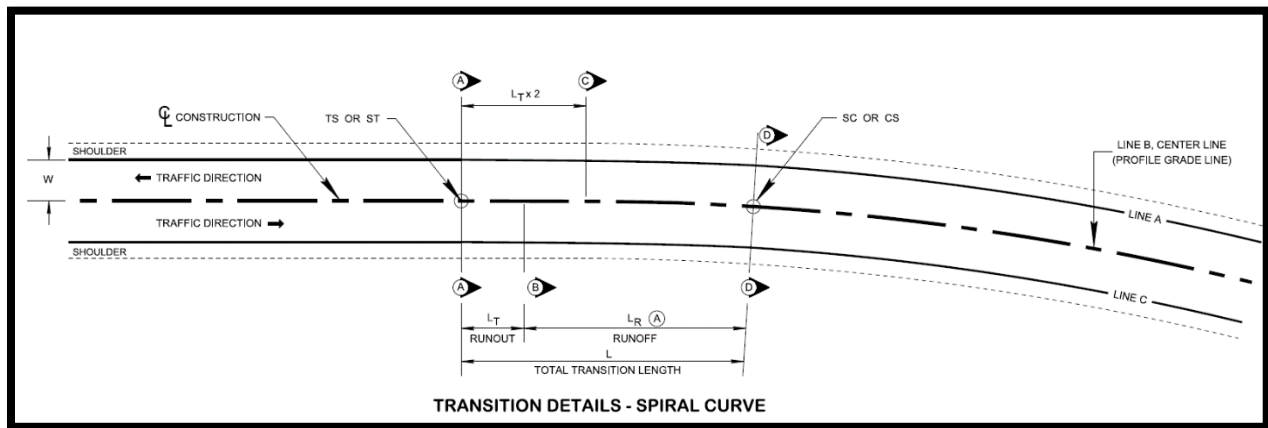
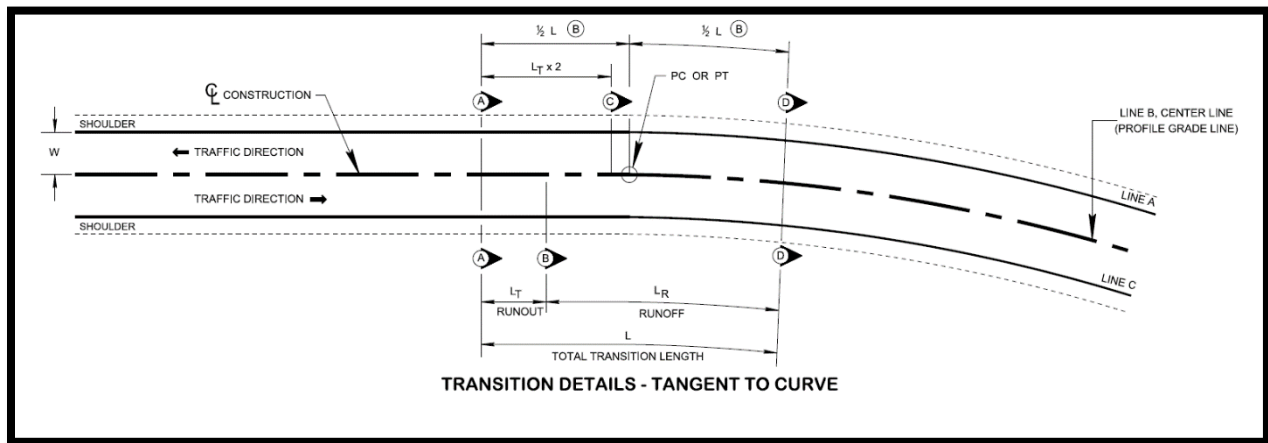
For example, given a radius of 730 ft., the corresponding super rate is 3%. If the e_d is to remain at 3%, any radius greater than 730 can be used. If the radius is to remain at 730, no other e_d than 3% can be used.

The numbers that appear under the number of lanes are runoff lengths (L_R). Runoff Length (L_R) is the distance that is required to transition from zero (flat) superelevation to full superelevation. The total transition length (L) is the length at which the transition from Normal Crown (NC) to full super (e_d) takes place.

The formula for the total transition length is found on Standard Drawing RD11-SE-1.

SUPERELEVATION TRANSITION EQUATIONS	
$L = L_R + L_T$	
$L_R = \frac{(W + 1) e_d}{\Delta \%} (b_w)$	
$L_T = \frac{NC}{e_d} L_R$	

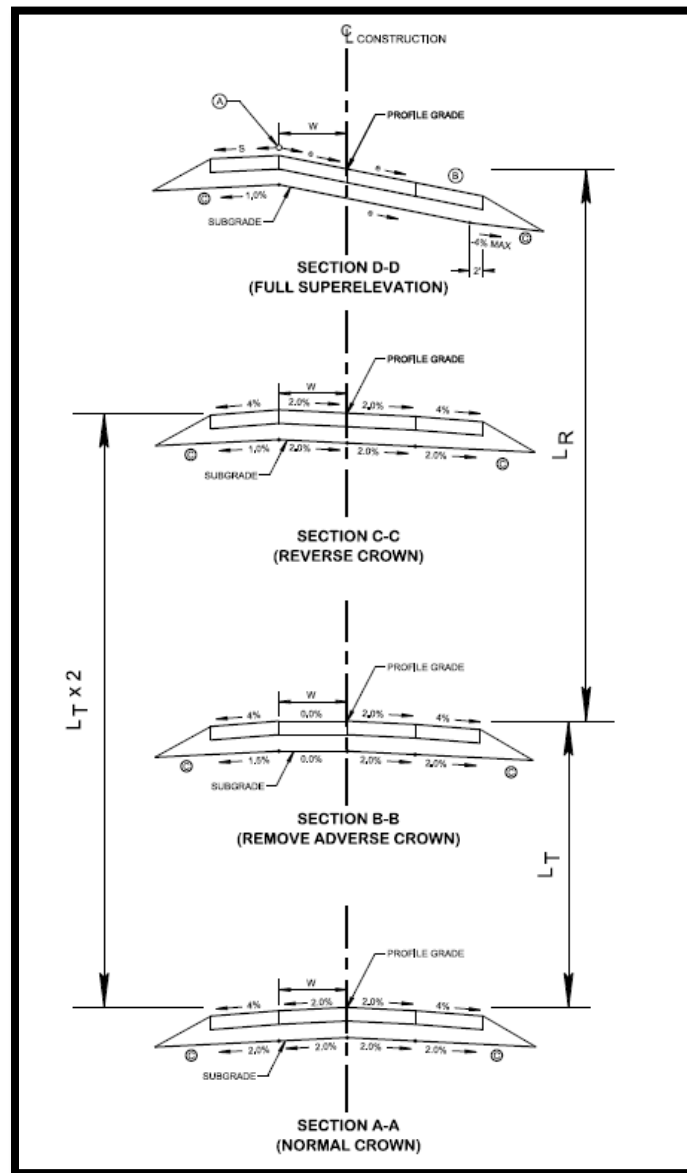
Standard Drawing RD11-SE-2 shows the relationship of L to the begin and end points of the horizontal curve.



For a simple curve half of the transition length is before and half after the P.C. or P.T.

For a spiral curve L is the same as the length of the spiral.

Standard Drawing RD11-SE-2A shows the lengths at which key points occur within the transition length.



NOTE: Standard Drawings RD11-SE-3 and 3A contain the same information as RD11-SE-2 and 2A, except for divided highways.

Example 1

- 2 lane rural design
- Design Speed 50 MPH
- Curve Radius 2280 ft.

According to Standard Drawing RD11-LR-2 (Minimum Runoff Lengths for Rural Highways), the superelevation rate (e_d) for this curve is 4.6% (.046 ft./ft.). 2280 ft. is the minimum radius that can be used with this rate. This also means that for a particular e_d rate a higher radius can be used.

DESIGN RUNOFF LENGTHS (L_R) ①

E MAX = 0.08 DESIRABLE

③ e _d [%] MIN. (FT.)	V = 20 (MPH)						V = 25 (MPH)						V = 30 (MPH)						V = 35 (MPH)						V = 40 (MPH)						V = 45 (MPH)						V = 50 (MPH)						V = 55 (MPH)					
	Number of lanes						Number of lanes						Number of lanes						Number of lanes						Number of lanes						Number of lanes						Number of lanes						Number of lanes					
	2	3	4	5	6	R	2	3	4	5	6	R	2	3	4	5	6	R	2	3	4	5	6	R	2	3	4	5	6	R	2	3	4	5	6	R	2	3	4	5	6	R						
NC	1640	0	0	0	0	0	2370	0	0	0	0	0	2440	0	0	0	0	0	4260	0	0	0	0	0	5410	0	0	0	0	0	6710	0	0	0	0	8150	0	0	0	0	9720	0	0					
2	1130	32	40	49	57	65	1720	24	43	51	60	69	2370	35	45	55	64	73	81	89	97	105	113	121	129	137	145	153	161	169	177	185	193	201	209	217	225	233	241	249	257	265	273	281	289			
2.2	1070	36	44	54	62	72	1550	28	47	57	66	76	2130	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350			
2.4	955	39	48	58	68	78	1400	31	51	62	72	83	1920	44	54	65	76	87	98	109	120	131	142	153	164	175	186	197	208	219	230	241	252	263	274	285	296	307	318	329	340	351	362	373	384	395		
2.6	872	42	52	63	74	85	1280	35	55	67	78	90	1760	47	59	71	83	95	107	119	131	143	155	167	179	191	203	215	227	239	251	263	275	287	299	311	323	335	347	359	371	383	395	407	419			
2.8	796	45	57	68	79	91	1170	38	60	72	84	96	1610	51	63	76	89	102	115	128	141	154	167	180	193	206	219	232	245	258	271	284	297	310	323	336	349	362	375	388	401	414	427	440	453			
3	730	49	61	73	85	98	1070	41	64	77	90	103	1480	55	68	82	95	109	123	137	151	165	179	193	207	221	235	249	263	277	291	305	319	333	347	361	375	389	403	417	431	445	459	473	487			
3.2	672	52	65	78	91	104	980	45	68	82	96	110	1350	59	72	87	101	115	130	144	158	172	186	200	214	228	242	256	270	284	298	312	326	340	354	368	382	396	410	424	438	452	466	480	494			
3.4	620	55	69	83	97	111	911	48	71	85	100	114	1280	62	77	92	107	122	137	152	167	182	197	212	227	242	257	272	287	302	317	332	347	362	377	392	407	422	437	452	467	482	497	512	527			
3.6	572	58	73	88	102	117	845	52	75	90	105	120	1350	65	80	95	110	125	140	155	170	185	200	215	230	245	260	275	290	305	320	335	350	365	380	395	410	425	440	455	470	485	500	515	530			
3.8	530	62	77	92	108	124	784	55	81	96	111	131	1300	69	84	99	114	129	144	159	174	189	204	219	234	249	264	279	294	309	324	339	354	369	384	399	414	429	444	459	474	489	504	519	534			
4	480	65	81	97	114	130	726	59	85	101	117	137	1280	73	90	106	122	138	154	170	186	202	218	234	250	266	282	298	314	330	346	362	378	394	410	426	442	458	474	490	506	522	538	554	570			
4.2	452	68	85	102	119	137	678	62	90	107	125	145	1350	76	94	112	130	148	166	184	202	220	238	256	274	292	310	328	346	364	382	400	418	436	454	472	490	508	526	544	562	580	598	616	634			
4.4	428	71	89	107	125	145	630	65	94	112	132	152	1280	80	100	120	140	160	180	200	220	240	260	280	300	320	340	360	380	400	420	440	460	480	500	520	540	560	580	600	620	640	660	680	700			
4.6	404	75	93	112	131	150	586	68	98	118	138	158	1230	84	104	124	144	164	184	204	224	244	264	284	304	324	344	364	384	404	424	444	464	484	504	524	544	564	584	604	624	644	664	684	704			
4.8	389	78	97	117	136	156	542	72	102	122	142	162	1180	88	108	128	148	168	188	208	228	248	268	288	308	328	348	368	388	408	428	448	468	488	508	528	548	568	588	608	628	648	668	688	708			
5	374	81	101	122	142	163	499	75	105	125	145	165	1130	92	112	132	152	172	192	212	232	252	272	292	312	332	352	372	392	412	432	452	472	492	512	532	552	572	592	612	632	652	672	692	712			
5.2	364	84	105	126	146	167	457	78	108	128	148	168	1080	96	116	136	156	176	196	216	236	256	276	296	316	336	356	376	396	416	436	456	476	496	516	536	556	576	596	616	636	656	676	696	716			
5.4	358	88	109	131	152	173	420	82	112	132	152	172	1030	100	120	140	160	180	200	220	240	260	280	300	320	340	360	380	400	420	440	460	480	500	520	540	560	580	600	620	640	660	680	700	720	740		
5.6	346	91	113	135	157	180	387	86	116	136	156	176	980	104	124	144	164	184	204	224	244	264	284	304	324	344	364	384	404	424	444	464	484	504	524	544	564	584	604	624	644	664	684	704	724	744		
5.8	336	94	117	141	165	189	358	89	119	139	159	179	930	108	128	148	168	188	208	228	248	268	288	308	328	348	368	388	408	428	448	468	488	508	528	548	568	588	608	628	648	668	688	708	728	748		
6	328	97	121	145	170	195	332	92	122	142	162	182	880	112	132	152	172	192	212	232	252	272	292	312	332	352	372	392	412	432	452	472	492	512	532	552	572	592	612	632	652	672	692	712	732	752		
6.2	324	101	125	151	176	202	308	96	126	146	166	186	830	116	136	156	176	196	216	236	256	276	296	316	336	356	376	396	416	436	456	476	496	516	536	556	576	596	616	636	656	676	696	716	736	756		
6.4	310	104	129	155	182	209	287	100	130	150	170	190	780	120	140	160	180	200	220	240	260	280	300	320	340	360	380	400	420	440	460	480	500	520	540	560	580	600	620	640	660	680	700	720	740	760	780	
6.6	307	107	133	161	190	220	267	103	133	153	173	193	740	124	144	164	184	204	224	244	264	284	304	324	344	364	384	404	424	444	464	484	504	524	544	564	584	604	624	644	664	684	704	724	744	764	784	

For instance, according to the table, a radius of 4400 ft. can be used with a superelevation rate of 4.6%.

In the table, the runoff lengths are given. For a rate of 4.6% and R = 2280, the runoff length (L_R) is 110 feet for 2 lanes.

V = 50 (MPH)						
R (FT.)	Number of lanes					R (FT.)
	2	3	4	5	6	
8150	0	0	0	0	0	9720
5990	48	60	72	84	96	7150
5400	53	66	79	92	106	6450
4910	58	72	86	101	116	5870
4490	62	78	94	109	125	5370
4130	67	84	101	118	135	4950
3820	72	90	108	126	145	4580
3550	77	96	115	134	154	4250
3300	82	102	122	143	164	3970
3090	86	108	130	151	174	3710
2890	91	114	137	160	183	3480
2720	96	120	144	168	193	3270
2560	101	125	151	176	203	3080
2410	106	131	158	185	212	2910
2280	110	137	166	193	222	2750
2160	115	143	173	202	232	2610
2040	120	149	180	210	241	2470
1920	125	155	187	218	251	2350

In Standard Drawing RD11-SE-1, the total transition length (L) is equal to $L_R + L_T$, where L_T is the Tangent Runout Length.

**SUPERELEVATION
TRANSITION EQUATIONS**

$$L = L_R + L_T$$

$$L_R = \frac{(Wn1) e_d}{\Delta \%} (b_w)$$

$$L_T = \frac{NC}{e_d} L_R$$

According to the equation on RD11-SE-1, L_T equals to 47.83 ($2/4.6 \times 110$), and the total transition length (L) would be $110 + 47.83 = \underline{157.83}$, rounded to 158 ft.

Going back to RD11-LR-2, note #2 at the bottom of the sheet says that spirals are recommended for design speeds of 50 MPH or greater and superelevation of 3% or greater. So, in our example L is also equal to spiral length.

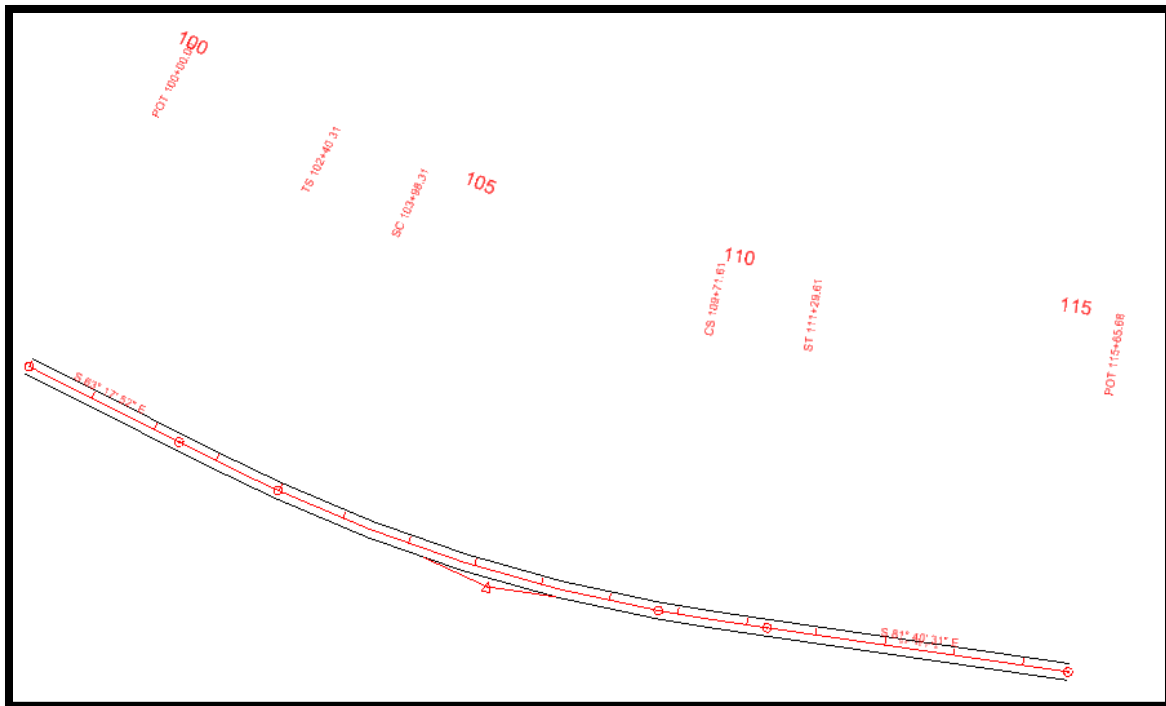
DESIGN RUNOFF LENGTHS (L_R)

IF MAX = 0.6% DESIRABLE

S	V = 20 (MPH)					V = 30 (MPH)					V = 40 (MPH)					V = 50 (MPH)					V = 60 (MPH)					V = 70 (MPH)					V = 80 (MPH)				
	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5					
0.1	10	15	20	25	30	15	20	25	30	35	20	25	30	35	40	25	30	35	40	45	30	35	40	45	50	35	40	45	50	55					
0.2	15	20	25	30	35	20	25	30	35	40	25	30	35	40	45	30	35	40	45	50	35	40	45	50	55	40	45	50	55	60					
0.3	20	25	30	35	40	25	30	35	40	45	30	35	40	45	50	35	40	45	50	55	40	45	50	55	60	45	50	55	60	65					
0.4	25	30	35	40	45	30	35	40	45	50	35	40	45	50	55	40	45	50	55	60	45	50	55	60	65	50	55	60	65	70					
0.5	30	35	40	45	50	35	40	45	50	55	40	45	50	55	60	45	50	55	60	65	50	55	60	65	70	55	60	65	70	75					
0.6	35	40	45	50	55	40	45	50	55	60	45	50	55	60	65	50	55	60	65	70	55	60	65	70	75	60	65	70	75	80					
0.7	40	45	50	55	60	45	50	55	60	65	50	55	60	65	70	55	60	65	70	75	60	65	70	75	80	65	70	75	80	85					
0.8	45	50	55	60	65	50	55	60	65	70	55	60	65	70	75	60	65	70	75	80	65	70	75	80	85	70	75	80	85	90					
0.9	50	55	60	65	70	55	60	65	70	75	60	65	70	75	80	65	70	75	80	85	70	75	80	85	90	75	80	85	90	95					
1.0	55	60	65	70	75	60	65	70	75	80	65	70	75	80	85	70	75	80	85	90	75	80	85	90	95	80	85	90	95	100					
1.1	60	65	70	75	80	65	70	75	80	85	70	75	80	85	90	75	80	85	90	95	80	85	90	95	100	85	90	95	100	105					
1.2	65	70	75	80	85	70	75	80	85	90	75	80	85	90	95	80	85	90	95	100	85	90	95	100	105	90	95	100	105	110					
1.3	70	75	80	85	90	75	80	85	90	95	80	85	90	95	100	85	90	95	100	105	90	95	100	105	110	95	100	105	110	115					
1.4	75	80	85	90	95	80	85	90	95	100	85	90	95	100	105	90	95	100	105	110	95	100	105	110	115	100	105	110	115	120					
1.5	80	85	90	95	100	85	90	95	100	105	90	95	100	105	110	95	100	105	110	115	100	105	110	115	120	105	110	115	120	125					
1.6	85	90	95	100	105	90	95	100	105	110	95	100	105	110	115	100	105	110	115	120	105	110	115	120	125	110	115	120	125	130					
1.7	90	95	100	105	110	95	100	105	110	115	100	105	110	115	120	105	110	115	120	125	110	115	120	125	130	115	120	125	130	135					
1.8	95	100	105	110	115	100	105	110	115	120	105	110	115	120	125	110	115	120	125	130	115	120	125	130	135	120	125	130	135	140					
1.9	100	105	110	115	120	105	110	115	120	125	110	115	120	125	130	115	120	125	130	135	120	125	130	135	140	125	130	135	140	145					
2.0	105	110	115	120	125	110	115	120	125	130	115	120	125	130	135	120	125	130	135	140	125	130	135	140	145	130	135	140	145	150					
2.1	110	115	120	125	130	115	120	125	130	135	120	125	130	135	140	125	130	135	140	145	130	135	140	145	150	135	140	145	150	155					
2.2	115	120	125	130	135	120	125	130	135	140	125	130	135	140	145	130	135	140	145	150	135	140	145	150	155	140	145	150	155	160					
2.3	120	125	130	135	140	125	130	135	140	145	130	135	140	145	150	135	140	145	150	155	140	145	150	155	160	145	150	155	160	165					
2.4	125	130	135	140	145	130	135	140	145	150	135	140	145	150	155	140	145	150	155	160	145	150	155	160	165	150	155	160	165	170					
2.5	130	135	140	145	150	135	140	145	150	155	140	145	150	155	160	145	150	155	160	165	150	155	160	165	170	155	160	165	170	175					
2.6	135	140	145	150	155	140	145	150	155	160	145	150	155	160	165	150	155	160	165	170	155	160	165	170	175	160	165	170	175	180					
2.7	140	145	150	155	160	145	150	155	160	165	150	155	160	165	170	155	160	165	170	175	160	165	170	175	180	165	170	175	180	185					
2.8	145	150	155	160	165	150	155	160	165	170	155	160	165	170	175	160	165	170	175	180	165	170	175	180	185	170	175	180	185	190					
2.9	150	155	160	165	170	155	160	165	170	175	160	165	170	175	180	165	170	175	180	185	170	175	180	185	190	175	180	185	190	195					
3.0	155	160	165	170	175	160	165	170	175	180	165	170	175	180	185	170	175	180	185	190	175	180	185	190	195	180	185	190	195	200					
3.1	160	165	170	175	180	165	170	175	180	185	170	175	180	185	190	175	180	185	190	195	180	185	190	195	200	185	190	195	200	205					
3.2	165	170	175	180	185	170	175	180	185	190	175	180	185	190	195	180	185	190	195	200	185	190	195	200	205	190	195	200	205	210					
3.3	170	175	180	185	190	175	180	185	190	195	180	185	190	195	200	185	190	195	200	205	190	195	200	205	210	195	200	205	210	215					
3.4	175	180	185	190	195	180	185	190	195	200	185	190	195	200	205	190	195	200	205	210	195	200	205	210	215	200	205	210	215	220					
3.5	180	185	190	195	200	185	190	195	200	205	190	195	200	205	210	195	200	205	210	215	200	205	210	215	220	205	210	215	220	225					
3.6	185	190	195	200	205	190	195	200	205	210	195	200	205	210	215	200	205	210	215	220	205	210	215	220	225	210	215	220	225	230					
3.7	190	195	200	205	210	195	200	205	210	215	200	205	210	215	220	205	210	215	220	225	210	215	220	225	230	215	220	225	230	235					
3.8	195	200	205	210	215	200	205	210	215	220	205	210	215	220	225	210	215	220	225	230	215	220	225	230	235	220	225	230	235	240					
3.9	200	205	210	215	220	205	210	215	220	225	210	215	220	225	230	215	220	225	230	235	220	225	230	235	240	225	230	235	240	245					
4.0	205	210	215	220	225	210	215	220	225	230	215	220	225	230	235	220	225	230	235	240	225	230	235	240	245	230	235	240	245	250					
4.1	210	215	220	225	230	215	220	225	230	235	220	225	230	235	240	225	230	235	240	245	230	235	240	245	250	235	240	245	250	255					
4.2	215	220	225	230	235	220	225	230	235	240	225	230	235	240	245	225	230	235	240	245	230	235	240	245	250	235	240	245	250	255					
4.3	220	225	230	235	240	225	230	235	240	245	230	235	240	245	250	235	240	245	250	255	240	245	250	255	260	245	250	255	260	265					
4.4	225	230	235	240	245	230	235	240	245	250	235	240	245	250	255	240	245	250	255	260	245	250	255	260	265	250	255	260	265	270					
4.5	230	235	240	245	250	235	240	245	250	255	240	245	250	255	260	245	250	255	260	265	250	255	260	265	270	255	260	265	270	275					
4.6	235	240	245	250	255	240	245	250	255	260	245	250	255	260	265	250	255	260	265	270	255	260	265	270	275	260	265	270	275						

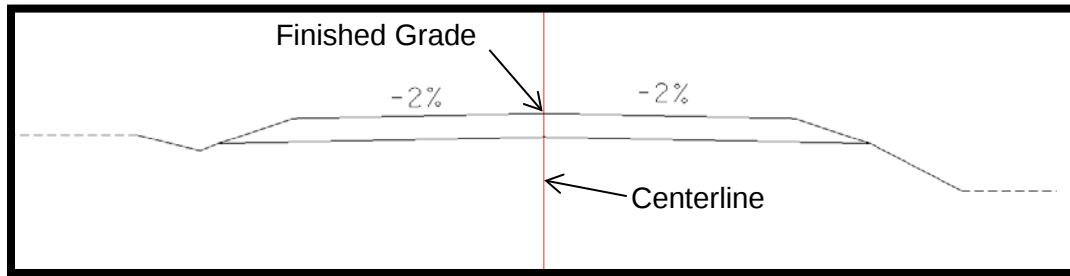
Plan view of proposed alignment

Station 100+00	Alignment Begins
Station 102+40.31	T.S. of the curve
Station 103+98.31	S.C. of the curve
Station 109+71.61	C.S. of the curve
Station 111+29.61	S.T. of the curve
Station 115+65.68	Alignment Ends



Normal Crown

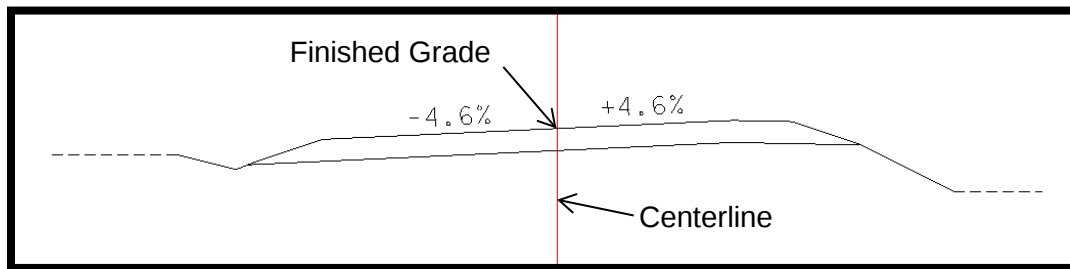
The alignment starts out at normal crown at station 100+00.



Full Superelevation

The transition to superelevation will begin at the T.S. point, station 102+40.31.

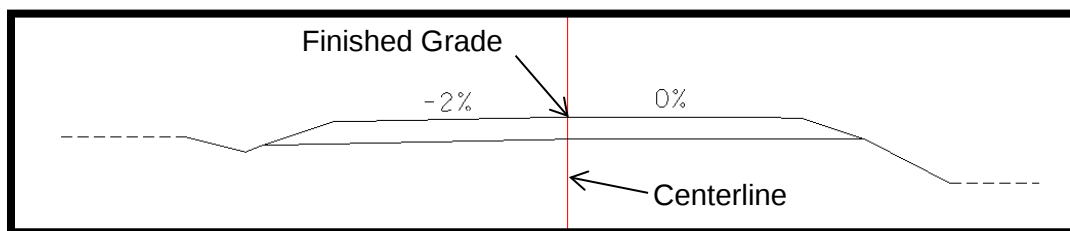
The transition ends at the S.C. point, station 103+98.31. This is the station at which full superelevation begins.



Remove Adverse Crown

In the transition area a couple of key points to know are the Reverse Crown station and the Remove Adverse Crown station.

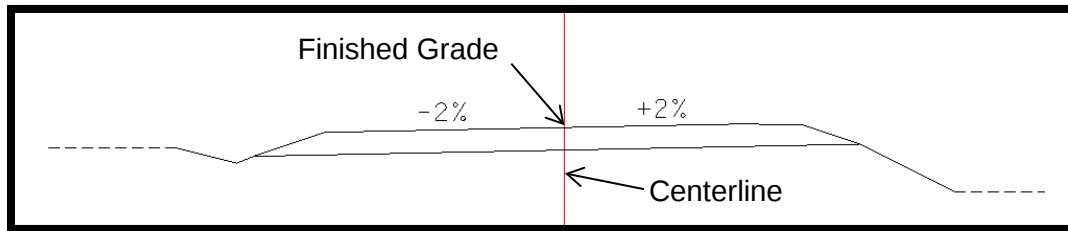
Going from Normal Crown to Full Super the point Remove Adverse Crown point will occur first.



Reverse Crown

Since the roadway curves to the left, the pavement transitions from a negative cross slope to a positive cross slope only on the right side, therefore zero cross slope would only be on the right side. According to RD11-SE-2A, this point occurs at the distance L_T from the T.S. station, or

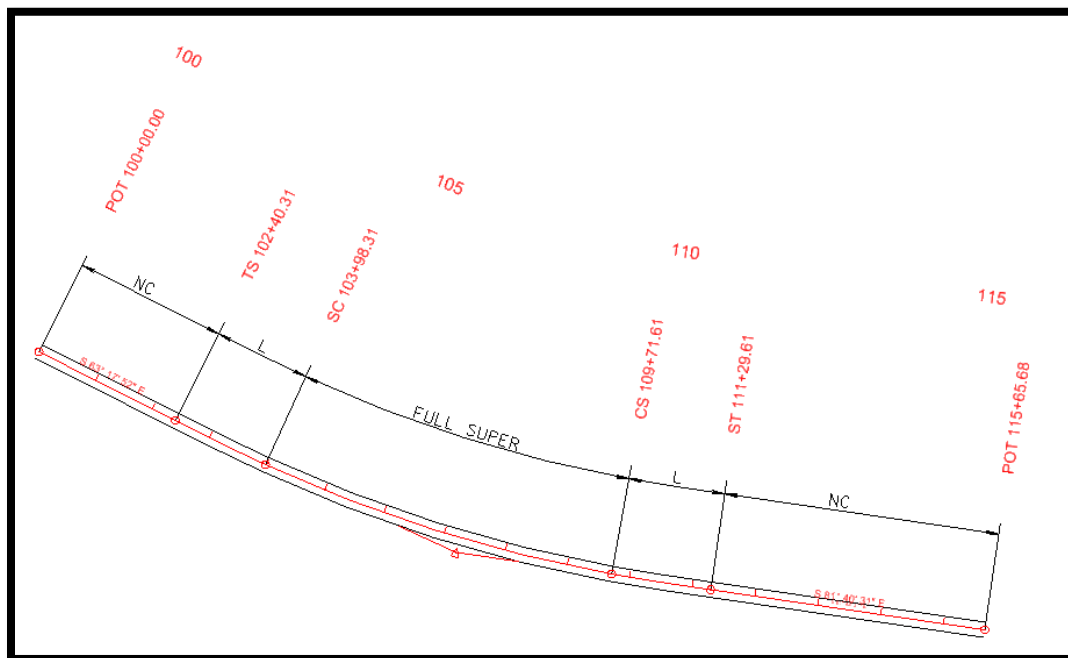
$$10240.31 + 47.83 = 10288.14, \text{ or station } \underline{102+88.14}$$



Also, from RD11-SE-2A, Reverse Crown occurs at T.S. + ($L_T \times 2$), or

$$10240.31 + (47.83 \times 2) = 10335.97, \text{ or station } \underline{103+35.97}$$

At the other end of the curve the alignment transitions from full super back to normal crown. The transition begins at the C.S. point (station 109+71.61) and ends at the S.T. point (station 111+29.61). The Reverse Crown and Zero Cross Slope stations would be calculated in the same manner as for the first transition and would occur in reverse order.



Now let's pick some random stations and calculate the superelevation:

103+00

This station occurs in the spiral portion of the alignment which is in the transition.

The rate of change in superelevation is found by dividing the difference between normal crown and full super by the transition length.

$$\text{For this example, } \frac{.046 - (-.020)}{158} = \frac{.066}{158} = .0004177$$

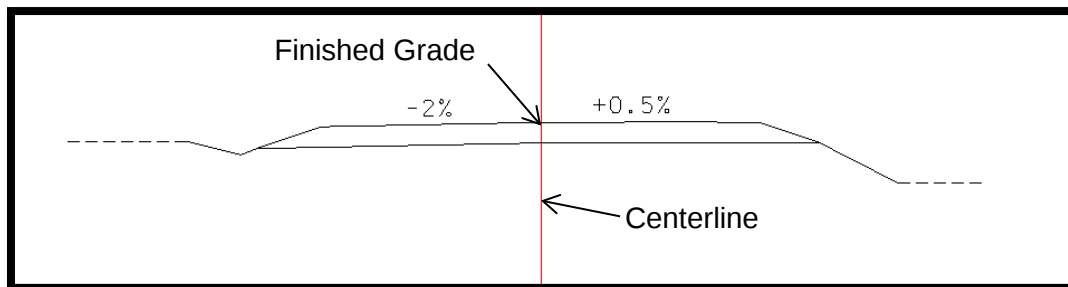
$$L = 10300 - 10240.31 = 59.69$$

$$59.69 \times .0004177 = .025, \text{ or } 2.5\%$$

This number is added to the cross slope at the beginning transition station, 102+40.31, which is normal crown (-2%)

$$2.5\% + (-2\%) = +0.5\%$$

Since this number is less than + 2%, and has not yet reached reverse crown, the other side will be - 2%



107+00

Station 107+00 is in the full super area, between the S.C and C.S. + 4.6% in this example.

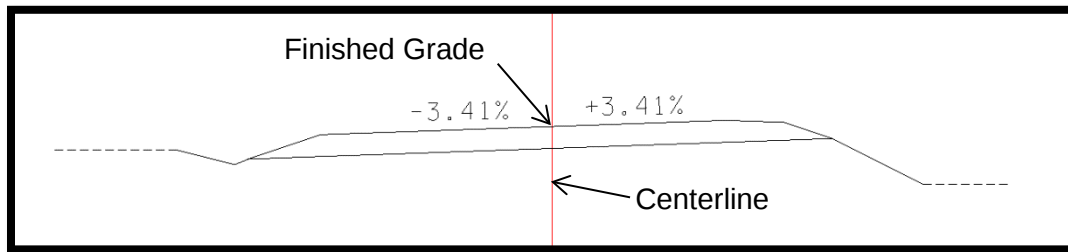
110+00

This station is in the transition from full super to normal crown (109+71.61 - 111+29.61), so subtract the beginning station of the transition

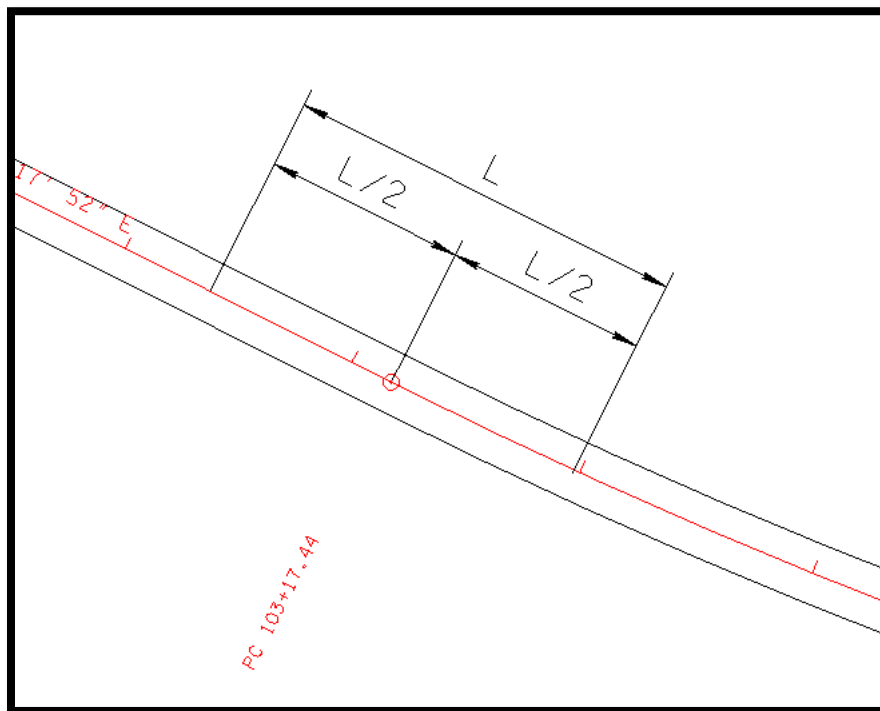
11000 - 10971.61 = 28.39. The rate of change is the same as for the transition at the beginning end of the curve (.0004177).

$$28.39 \times .0004177 = .0119, \text{ or } 1.19\%$$

This number is subtracted from the full super rate at 109+77.61, 4.6 -1.19 = 3.41%



For curves where a spiral is not required, the calculation methods are the same. The calculated transition lengths are spaced so that the P.C. and P.T. points are at the halfway point of L.



Example 2

- 4 lane rural design
- Design Speed 30 MPH
- Curve Radius 261 ft.

Find L

Use Standard Drawing RD11-LR-1, Minimum Runoff Lengths for Urban Highways, $E_{\max} = 0.04$.

From the Table, $e_d = 3\%$. This is the minimum superelevation rate for this radius.

According to the table on RD11-LR-1, L_R is 82 feet.

According to the Superelevation Transition equation on RD11-SE-1, L_T is 54.67

$$L = L_R + L_T = 82 + 54.67 = 136.67, \text{ rounded to } 137 \text{ feet}$$

A spiral curve is not required for this design speed so half of L is on either side of the P.C. or P.T. as shown on the previous page.

If the P.C. is at station 103+17.44:

Transition begins at $103+17.44 - (137/2) = 10248.94$, station 102+48.94

Remove Adverse Crown is $10248.94 + L_T = 10248.94 + 54.67 = 10303.61$, station 103+03.61

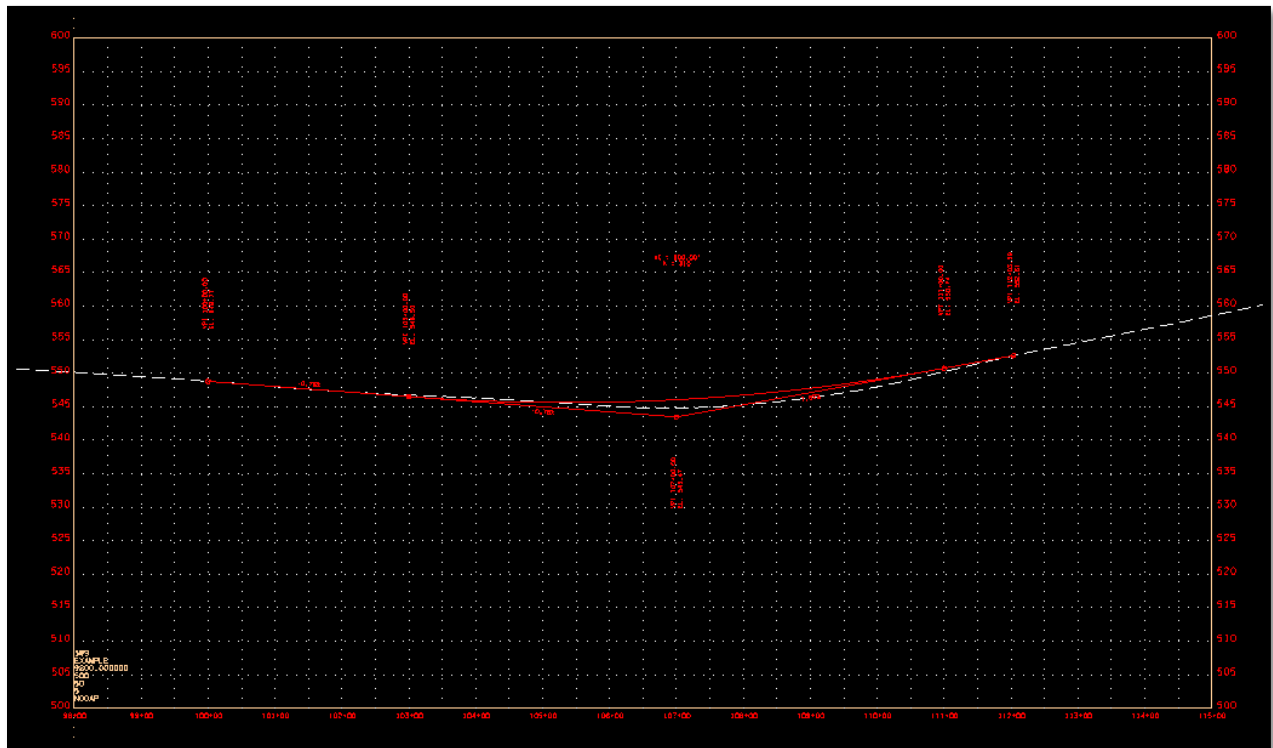
Reverse Crown is $10248.94 + 2 \times L_T = 10248.94 + 109.34 = 10358.28$, station 103+58.28

Part 4: Superelevation Profile Diagram

The purpose of this section is to provide the designer information to draw the superelevation diagram. This diagram is important to show so that it is easily seen where superelevation changes take place.

Superelevation Diagram Placement

The best place to draw the superelevation diagram is in the alignment file. If you have displayed the proposed vertical alignment and a profile grid (See GEOPAK v8i Road Course Guide), the diagram should go in the lower portion of this area.



Determining Critical Superelevation Stations

From the Superelevation Calculations tutorial (.inp file created when "Generate Superelevation Transitions" operation is performed in GEOPAK), the stations where superelevations change are as follows:

Left

ROADNAME 8.0000

filler line station / slope

100+00.000000 -2.0000

106+00.315956 -2.0000

106+87.588683 -6.8000 /* Curve D1 */

107+74.861410 -2.0000

112+03.385413 -2.0000

Right

ROADNAME -8.0000

filler line station / slope

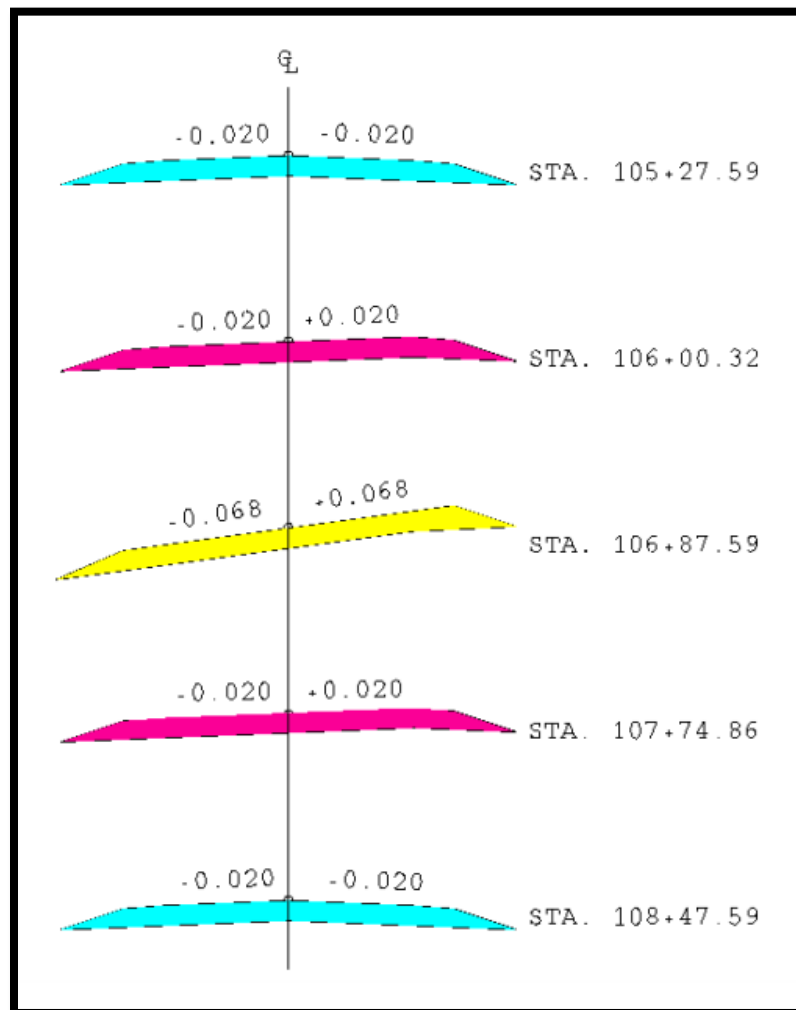
100+00.000000 -2.0000

105+27.588683 -2.0000

106+87.588683 6.8000 /* Curve D1 */

108+47.588683 -2.0000

112+03.390000 -2.0000



Drawing the Profile Diagram

Using the 510-elevation line on the grid, draw a line representing the finished grade which has a slope of 0% or 0 ft/ft.

Use the following symbology settings:

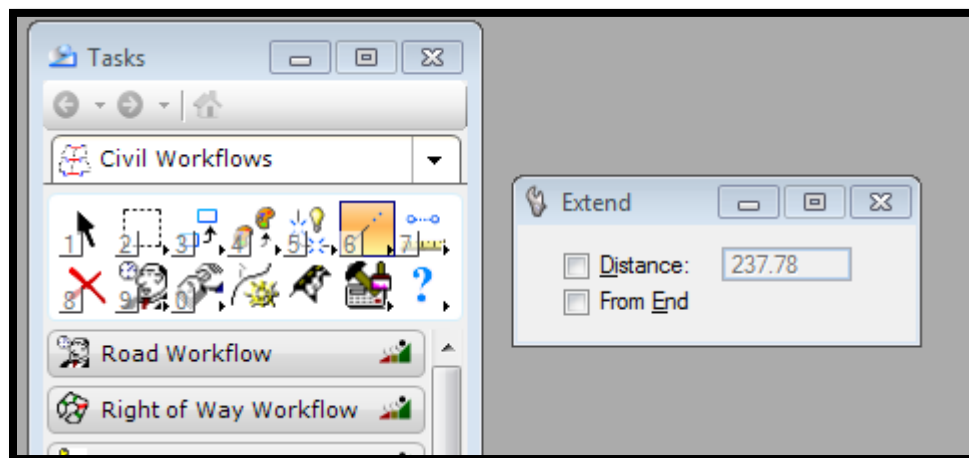
LV: DESIGN-CENTERLINE-Proposed Text

CO: 6

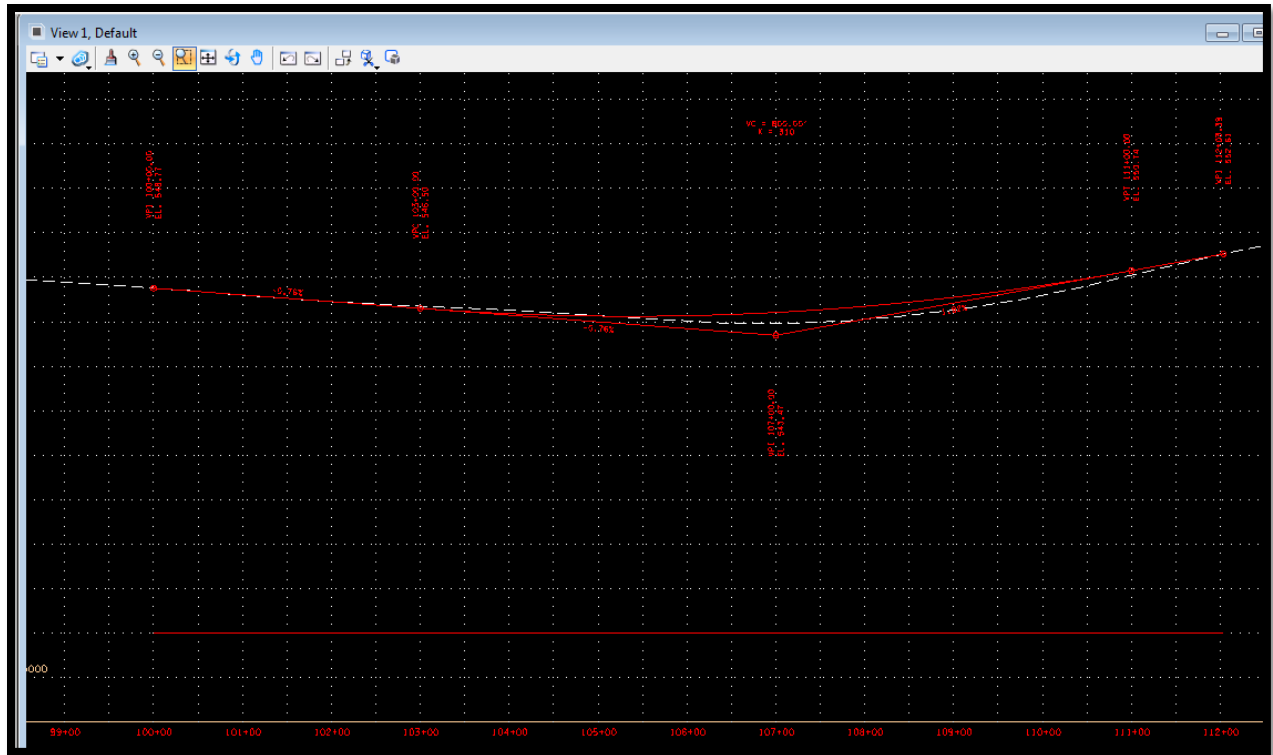
LC: 0

WT:10

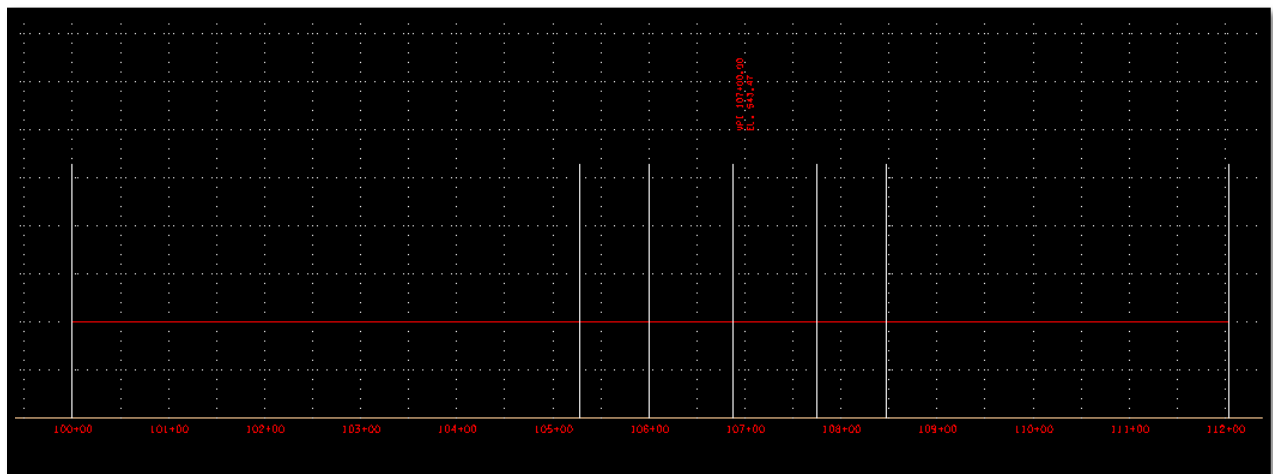
Make sure the line limits are the same as the proposed vertical grade. For this example, sta. 100+00 and sta. 112+03.39.



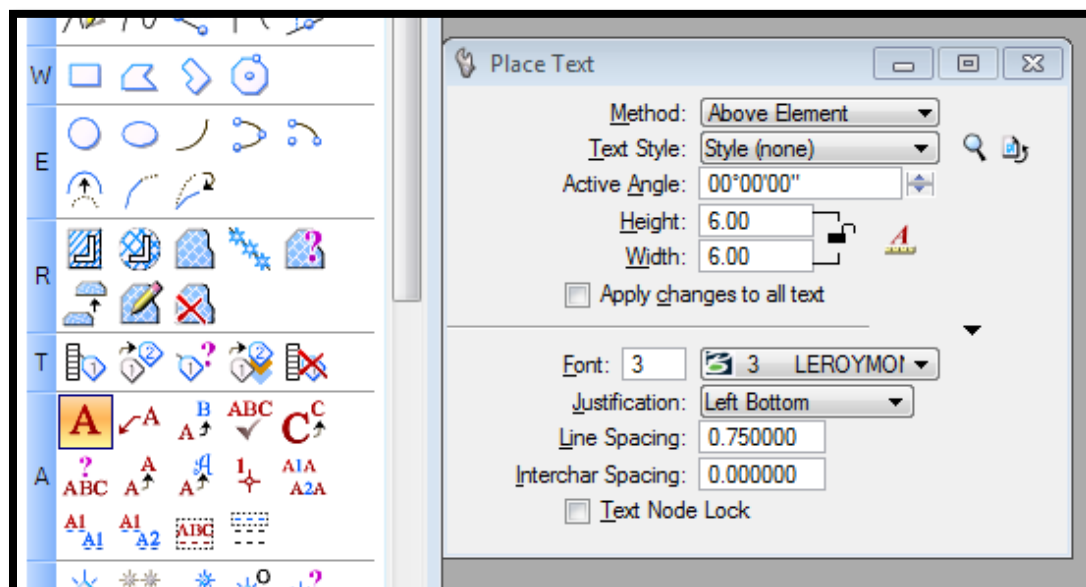
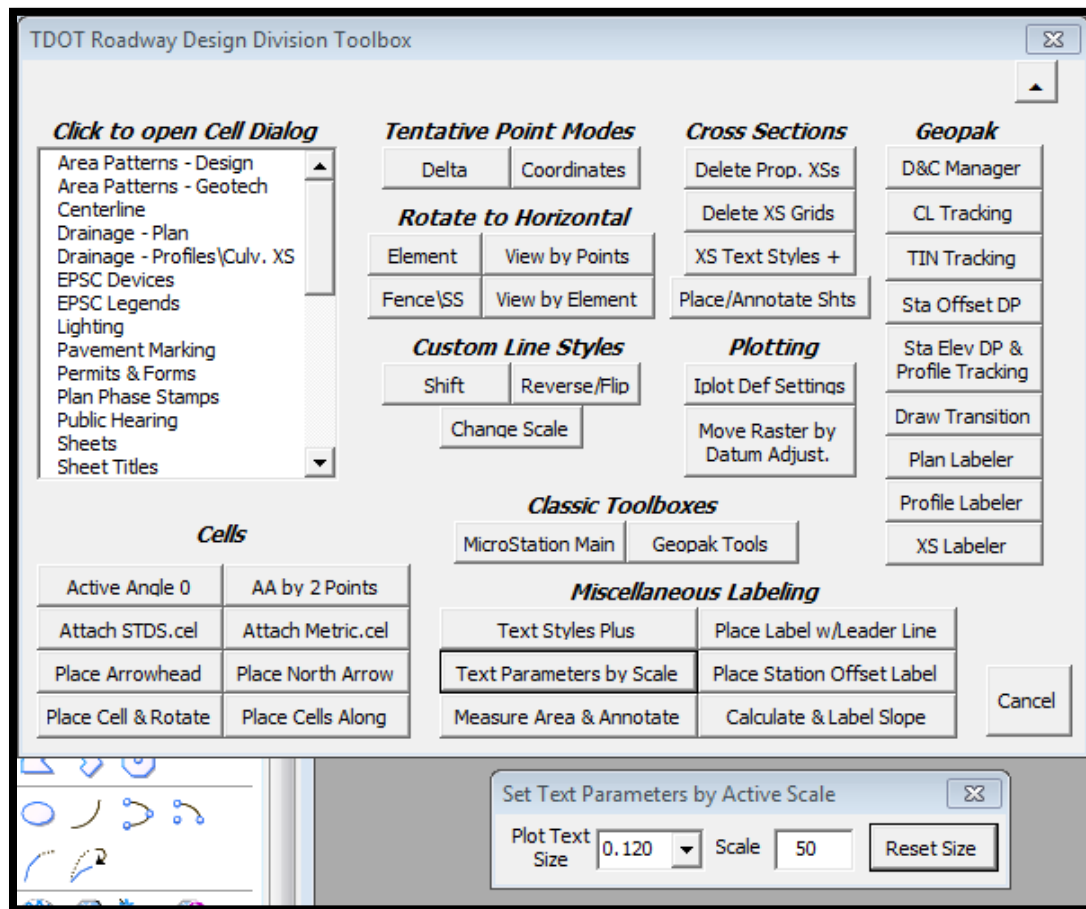
Use "Extend Line" and snap to each end of the profile.

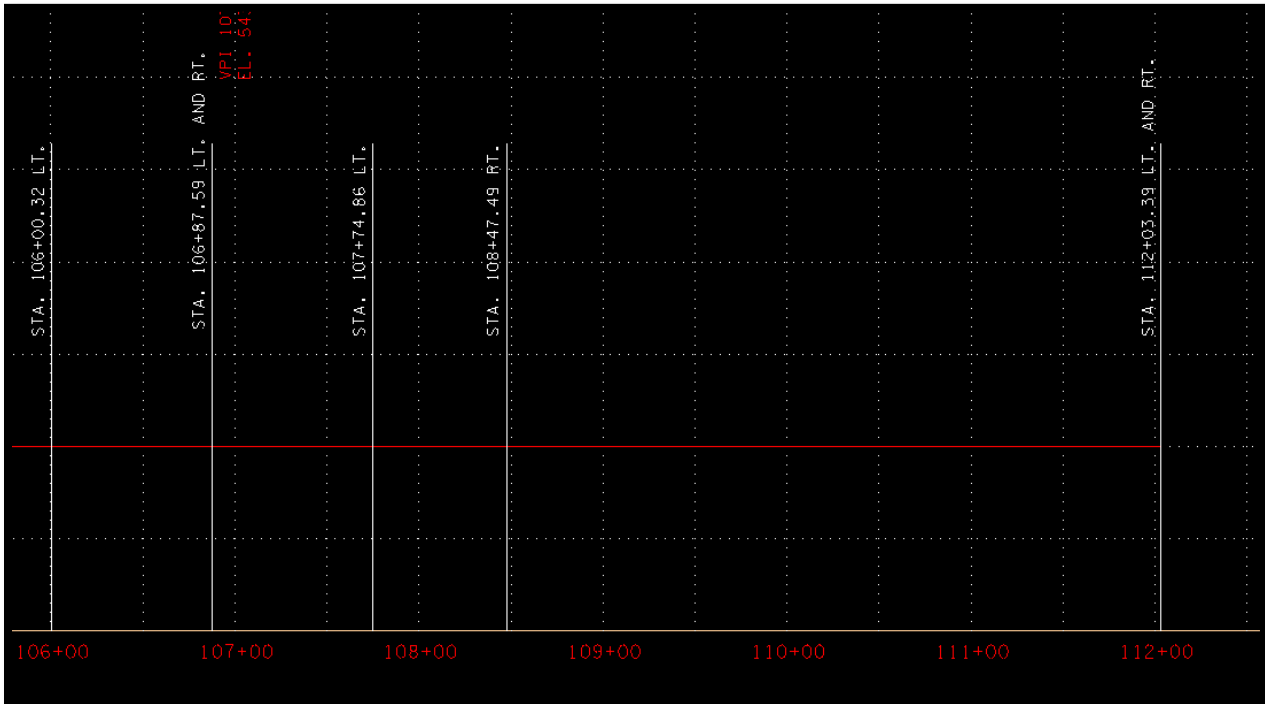
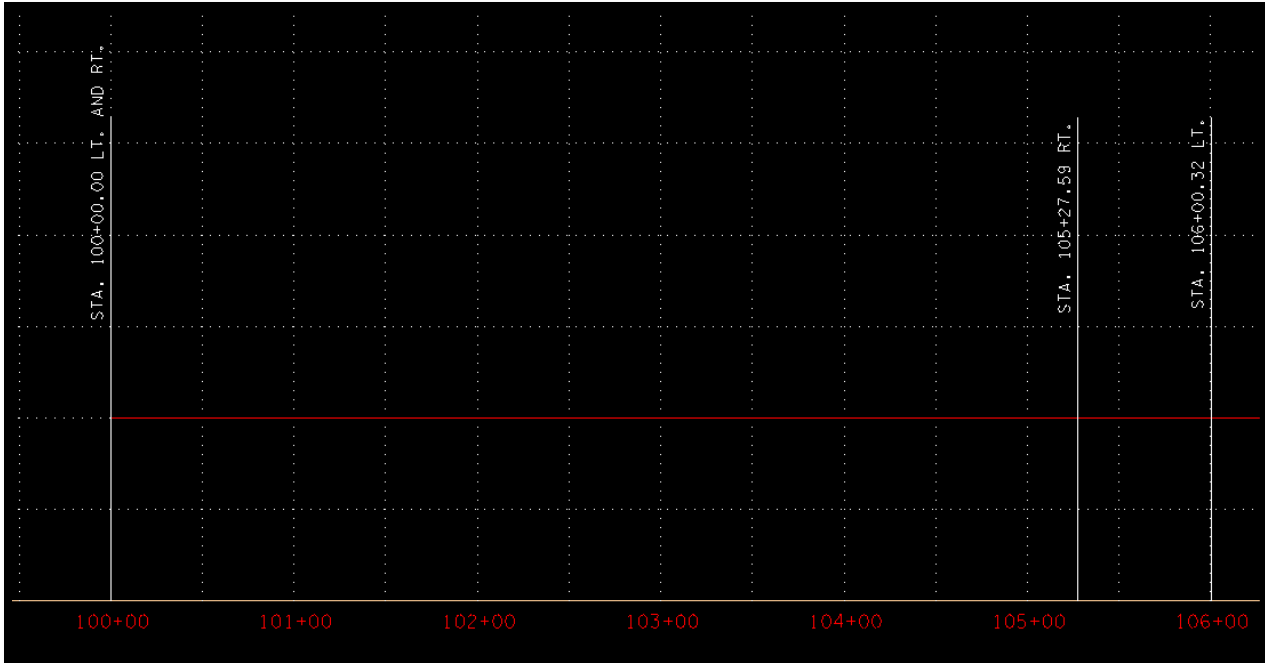


Change line symbology settings WT to 4 and CO to 0, draw vertical lines to represent the superelevation change stations listed on page 2 for both the right and left.



Make text settings as follows and label each vertical line as shown below:





Draw the Left Profile Diagram

To distinguish between the left and right diagrams, they should be drawn in different colors. For the left diagram, use the following settings:

LV: DESIGN-CENTERLINE-Proposed Text

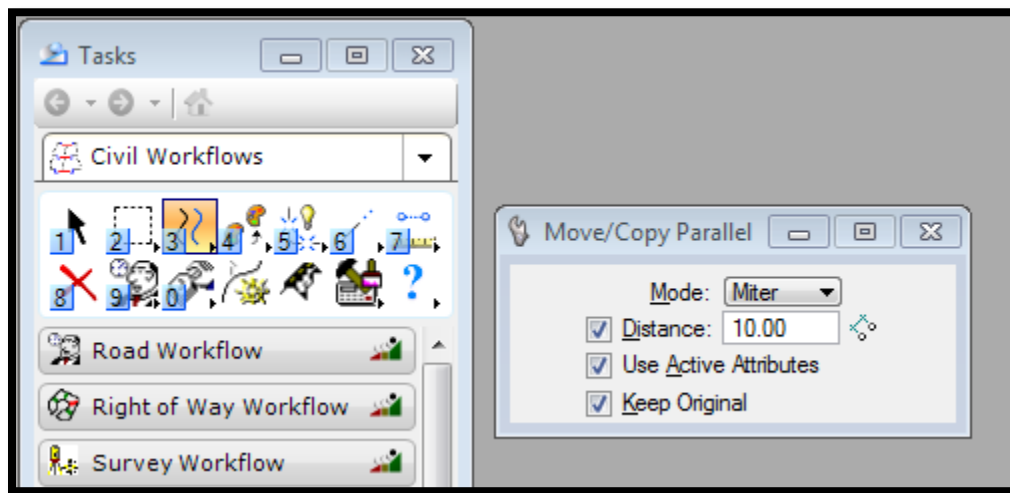
CO: 7

WT: 10

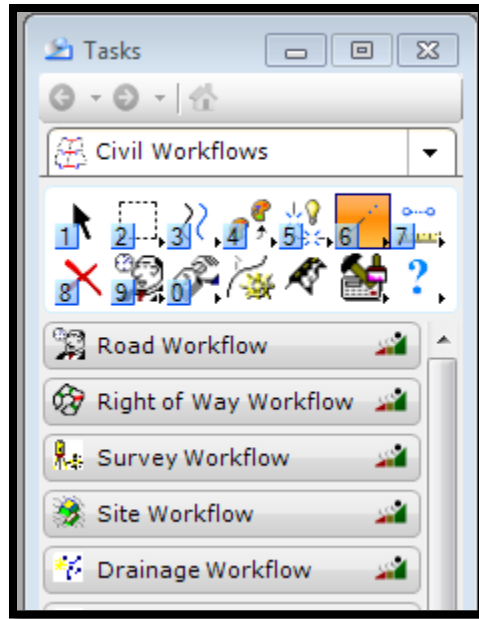
From sta. 100+00 to 106+00.32, the cross slope is a constant -2.00%, or -.020 ft/ft. To draw the diagram proportionally, set one vertical grid, 50 ft, equal to a maximum superelevation of 0.10 ft/ft. Therefore,

$$\frac{0.020 \text{ ft/ft} \times (50 \text{ ft})}{0.100 \text{ ft/ft}} = 10 \text{ ft}$$

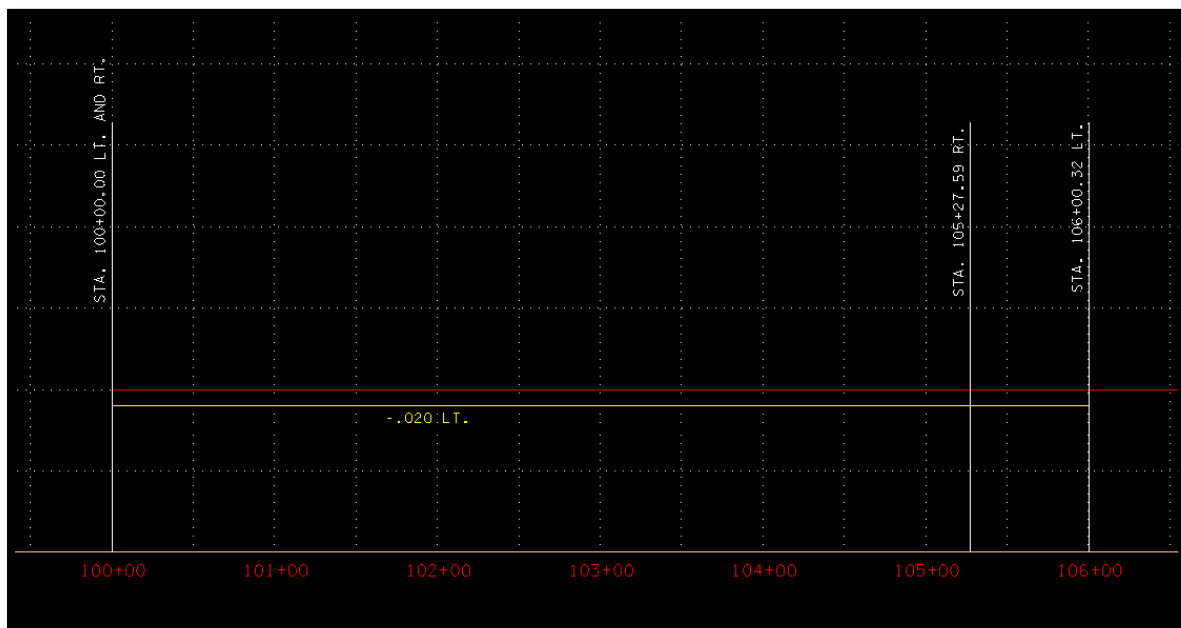
The line representing -.020 ft/ft superelevation for the left side can be drawn by copying parallel the red line drawn earlier using the settings:



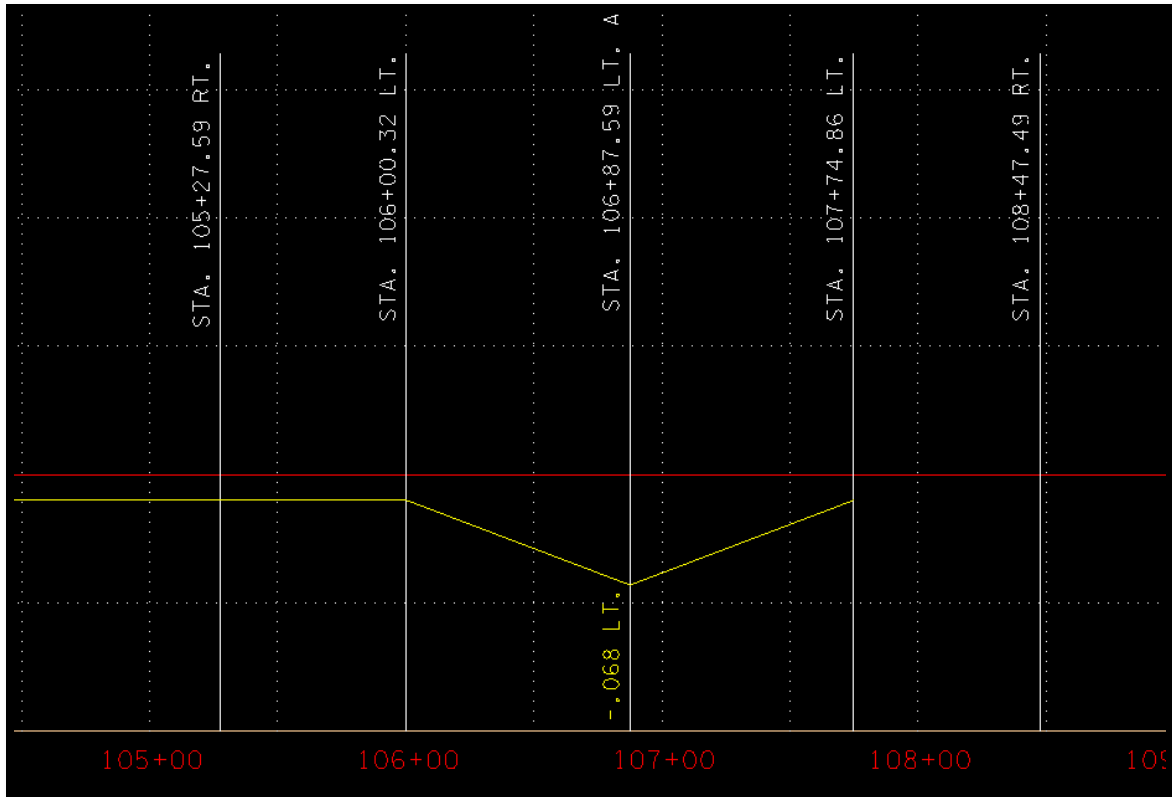
Make sure line ends at the sta. 106+00.32 line by using the “Lengthen or Shorten element to element” command:



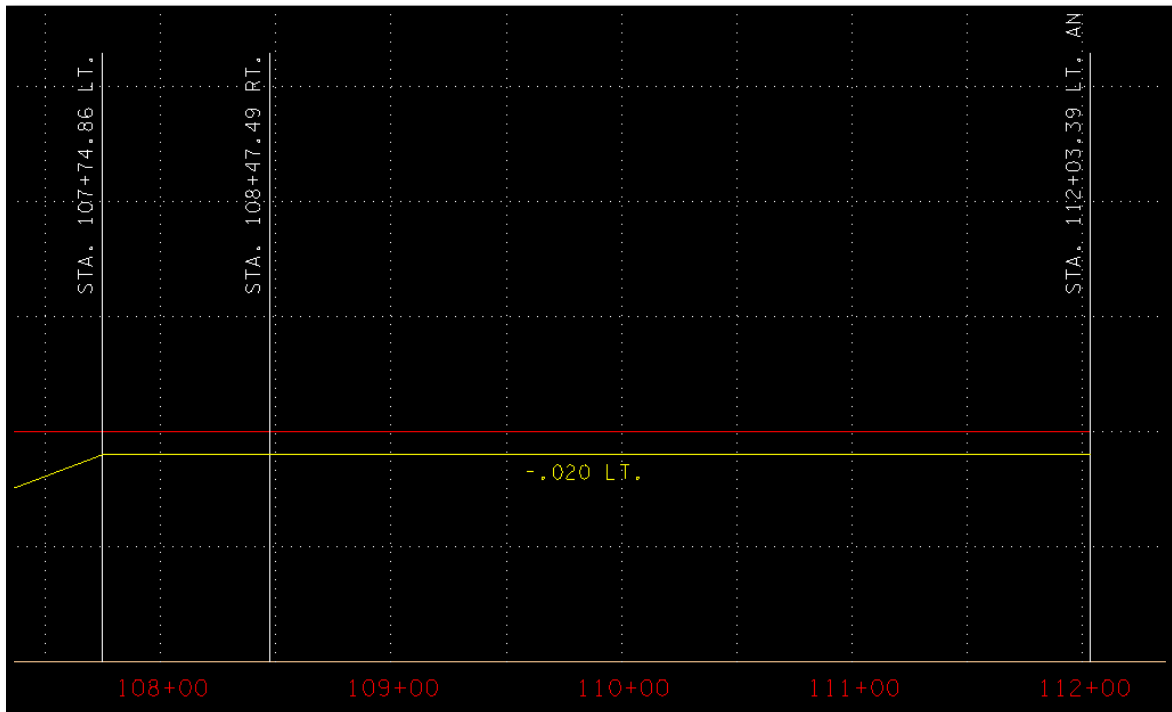
Label line as shown below using “Place text Under Element” option:



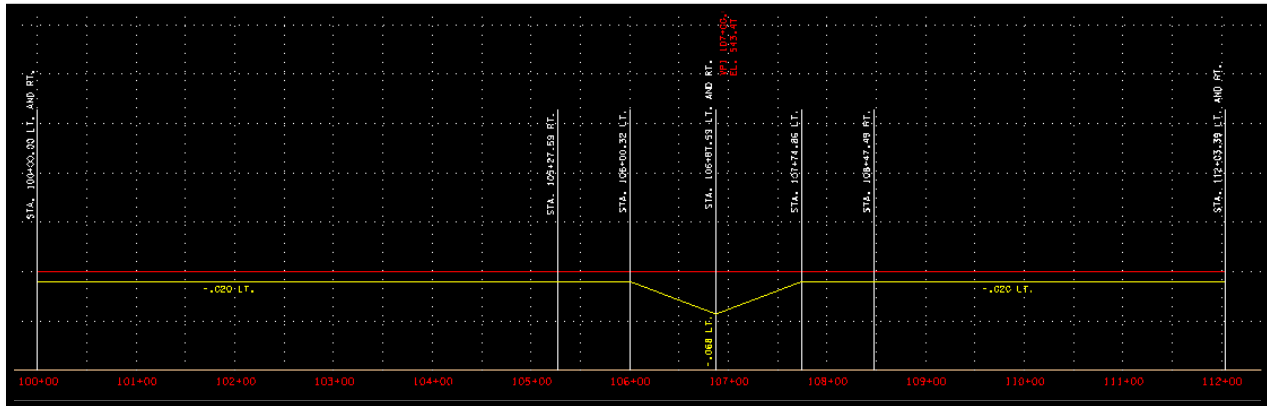
The next segment transitions from $-.020$ ft/ft at sta. 106+00.32 to $-.068$ ft/ft at sta. 106+87.59, then back to $-.020$ ft/ft at sta. 107+74.86. Using the same conversion on page 6, -0.068 ft/ft converts to 34 ft. below the red line. Label superelevation at sta. 106+87.59 as shown below using text settings as shown on page 5.



The last segment, from sta. 107+74.86 to sta. 112+03.39, has a constant slope of -0.020 ft/ft. Draw this segment and label similar to the first segment.



The diagram for the left side should look as shown:



Draw the Right Profile Diagram

Use the following symbology settings:

LV: DESIGN-CENTERLINE-Proposed Curve Text

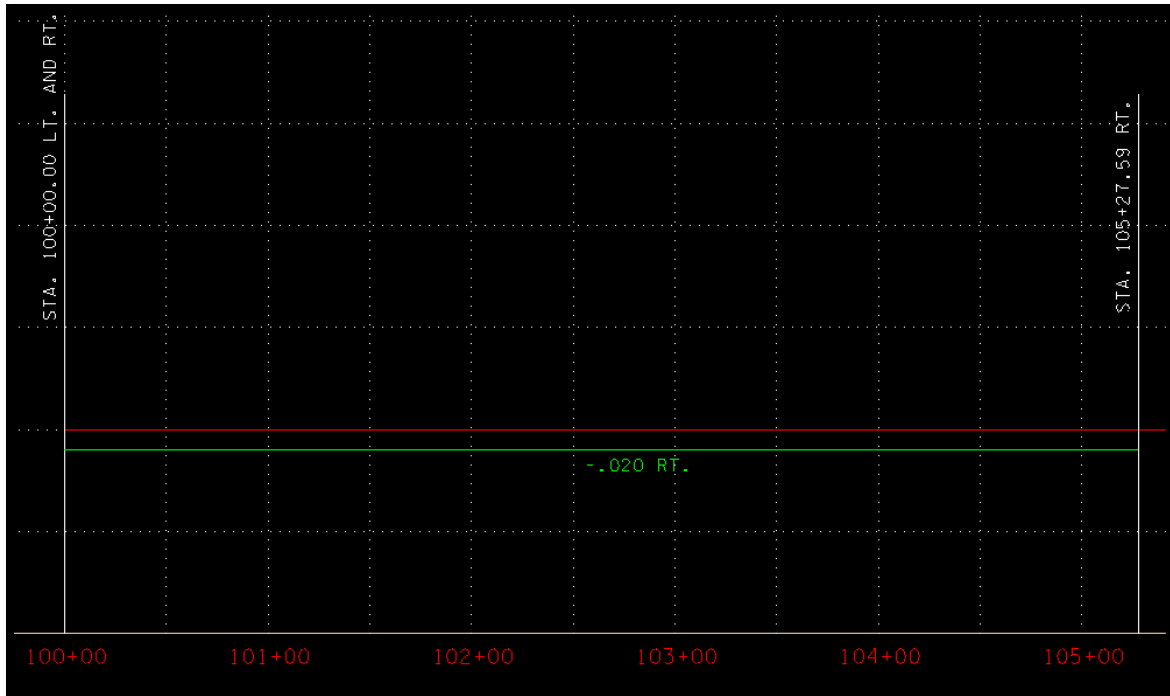
CO: 8

WT: 10

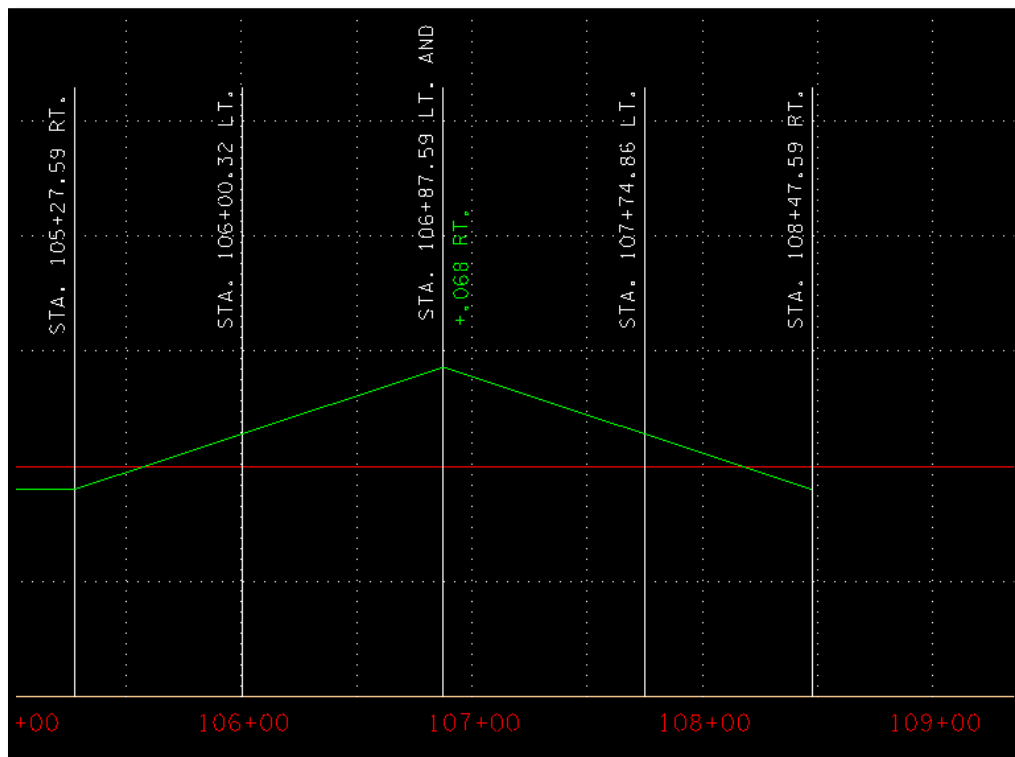
Before drawing the right-side diagram, turn off the level "DESIGN – PROFILE – Proposed Text", which was used for the left side diagram.

From sta. 100+00 to 105+27.59, the cross slope is a constant -0.020 ft/ft.

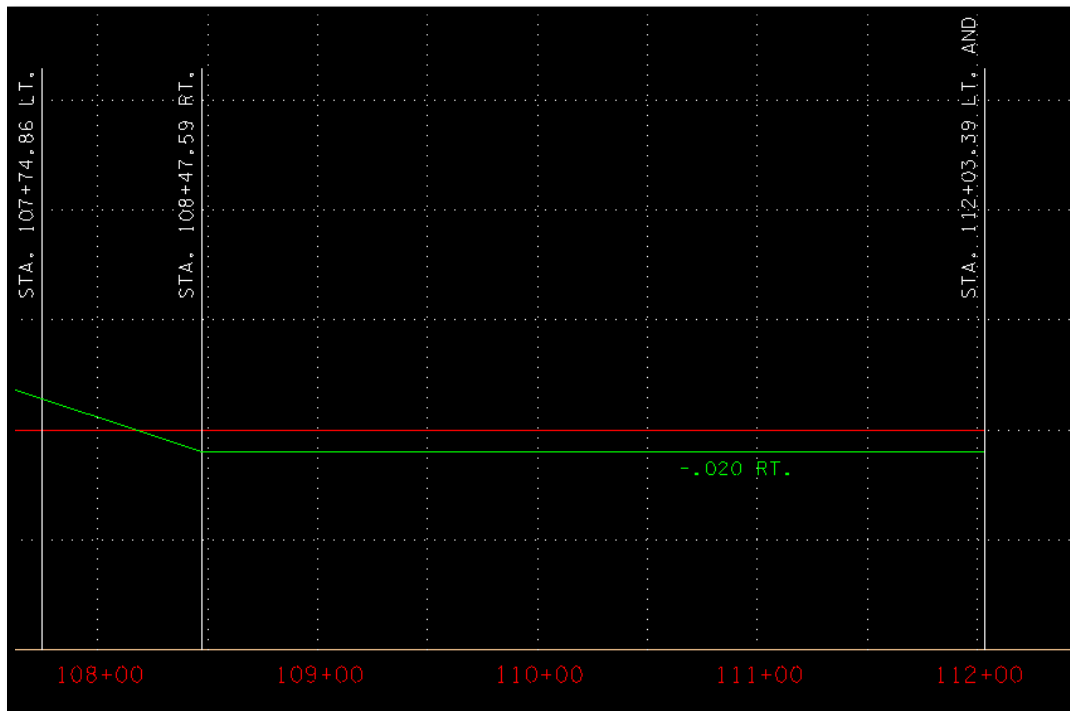
Similar to the left side diagram, copy parallel the line representing finished grade 10 ft below itself. Modify the new line to end at sta. 105+27.59.



The next segment transitions from -0.020 ft/ft at sta. 105+27.59 to $+0.068$ ft/ft at sta. 106+87.59, then back to -0.020 ft/ft at sta. 108+47.59. Using the same conversion on page 6, $+0.068$ ft/ft converts to 34 ft. above the red line. Label superelevation at sta. 106+87.59 as shown below using text settings as shown on page 5.



The last segment, from sta. 108+47.59 to sta. 112+03.39, has a constant slope of -0.020 ft/ft. Draw this segment and label similar to the first segment



Turn the level “DESIGN-PROFILE-Proposed Text” back on and the finished product should look like this:

