# Denitrification in Activated Sludge Processes

# Larry W. Moore

TN Plant Optimization Program (TNPOP)

# Organisms and Their Sources of Energy (or Food)

• Heterotrophic - use organic carbon

- CBOD removing organisms
- Denitrifying organisms
- Bio-P organisms
- Autotrophic use inorganic carbon
  Nitrifying organisms

# Organisms and Their Means of Respiration

- Aerobic use elemental oxygen
- Anoxic use nitrate (NO<sub>3</sub>) or nitrite (NO<sub>2</sub>)
- Anaerobic use other terminal electron acceptors (SO<sub>4</sub>, CO<sub>2</sub>) or none at all
- Facultative two or more means of respiration
- Fermentative no terminal electron acceptor

Terminal Electron Acceptors and Their Products

- Oxygen ( $O_2$ )  $\rightarrow$  H<sub>2</sub>O and CO<sub>2</sub>
- Nitrate  $(NO_3^-) \rightarrow N_2$ ,  $H_2O$ , and  $CO_2$
- Sulfate  $(SO_4^{=}) \rightarrow H_2S, H_2O, \text{ and } CO_2$

• Carbon dioxide (CO<sub>2</sub>)  $\rightarrow$  CH<sub>4</sub>, H<sub>2</sub>O, and CO<sub>2</sub>

## Denitrification

- Heterotrophic
- Anoxic (facultative)

## Adding an Anoxic Zone



#### **Comments about Anoxic Zone**

#### **Requirements:**

- Mixed, but un-aerated
- Nitrification in aerobic zone
- Mixed liquor recycle

#### **Comments about Anoxic Zone**

#### Uses:

- Nitrogen removal
- Alkalinity recovery
- CBOD removal (some)

Biological Nitrogen Removal is Optimized by an Environment that ...

- Provides the right source of energy
- Ensures the right means of respiration

## Minimizing DO in Anoxic Zone

- Avoid aeration at the inlet zone
  - don't allow a cascading influent
  - eliminate primary effluent flow splitting turbulence
- Eliminate mixer vortex if possible
- Avoid back mixing from the aerobic zone

#### **Effect of DO on Denitrification Rates**

<u>DO Conc, mg/L</u>	<b>Denitrification Rate</b>
0.0	100%
0.1	40%
0.2	20%
0.3	10%
> 0.3	Negligible

# Denitrification: Biochemical Reactions

Methanol as external carbon source:

 $6NO_3^{-} + 5CH_3OH \rightarrow 3N_2 + 5CO_2 + 7H_2O + 6OH^{-}$ 

## **Denitrification Reactions**

For one gram of NO<sub>3</sub>-N that is denitrified:

2.47 g of methanol (~3.7 g of COD) are consumed

0.45 g of new cells are produced

3.57 g of alkalinity are formed

TN Plant Optimization Program (TNPOP)

# Denitrification: Biochemical Reactions

Sewage as carbon source:

 $C_{10}H_{19}O_3N + 10NO_3^{-} \rightarrow 5N_2 + 10CO_2 + 3H_2O + 10OH^{-} + NH_3$ 

## **Factors Affecting Denitrification**

- Substrate degradability
- pH
- Dissolved oxygen
- Temperature

## **Oxygen Savings with Denitrification**

For every gram of NO<sub>3</sub>-N that is reduced to nitrogen gas, 2.86 grams of oxygen are saved.

#### **Comments about Denitrification**

 Rate of denitrification depends on nature and concentration of the carbonaceous organics being degraded

Rate<sub>methanol</sub> ≥ Rate<sub>sewage</sub> >> Rate<sub>endog resp</sub>

 Denitrification is a zero order reaction with respect to nitrate down to very low nitrate concentrations

TN Plant Optimization Program (TNPOP)

# Single-Sludge Denitrification

- To avoid the operating costs of using methanol as the carbon source, it is more cost-effective to use the organics available in raw sewage.
- These systems are referred to as "combined carbon oxidation / nitrification / denitrification" or "single-sludge."
- These systems have lower capital and operating costs than separate stage nitrification / denitrification systems

## **Single-Sludge** Denitrification

Two carbon sources are used:

- Endogenous decay of the activated sludge microbes
- Wastewater influent to the activated sludge process

## **Single-Sludge** Denitrification

Advantages:

- It uses only one clarifier
- No external carbon source is required
- It has lower neutralization chemical requirements
- It has lower oxygen requirements

**Disadvantage:** 

Need for pumping equipment and energy for recycling high volumes of mixed liquor

# Single-Sludge Denitrification Using Endogenous Decay



Single-Sludge Denitrification Using Endogenous Decay

**Disadvantages:** 

- Very low denitrification rate due to relatively low availability of carbon from endogenous decay and in the secondary effluent
- Potential for some ammonia-N release due to the decay and lysis of biomass
- Need a large anoxic reactor because of low denitrification rate

# Single-Sludge Denitrification Using Influent Organic Content



# Single-Sludge Denitrification Using Influent Organic Content

- Many process configurations
- Minimizes ammonia-N release
- Higher denitrification rate
- Uses alternating aerobic/anoxic zones

Single-Sludge Denitrification Using Influent Organic Content

**Expected Effluent Quality:** 

BOD<sub>5</sub> TSS Ammonia-N NO<sub>x</sub>-N Total N 5 - 15 mg/L 10 - 20 mg/L < 1 mg/L 5 - 7 mg/L 6 - 10 mg/L

#### Four Stage Bardenpho Process



## Four Stage Bardenpho Process

- Uses both wastewater carbon and endogenous decay carbon for denitrification
- Carbon present in raw waste is used to denitrify the recycled nitrate in first anoxic zone
- Ammonia in raw waste passes through first anoxic zone to be nitrified in first aerobic zone
- Nitrified mixed liquor flows from first aerobic zone to be denitrified at lower rate in second anoxic zone (endog resp)
- Final aerobic zone allows release of N<sub>2</sub> gas, improves sludge settleability, and oxidizes residual ammonia-N 27 of 42 **Denitrification in Activated Sludge Processes**

#### Four Stage Bardenpho Process

Expected Effluent Quality:

BOD<sub>5</sub> TSS Ammonia-N NO<sub>x</sub>-N Total N 5 - 15 mg/L 10 - 20 mg/L < 1 mg/L 1 - 3 mg/L 2 - 5 mg/L

# Modifying Existing WWTPs to Achieve Nitrogen Removal

# Performance of Single-Sludge Denitrification

- Can achieve high N removals (85% to 95%)
- Does not necessarily enhance sludge settleability in final clarifier
- Uses carbon source in influent
- Reduces the energy requirements for BOD removal from the wastewater (2.86 lb O<sub>2</sub> equivalent per lb of NO<sub>3</sub>-N removed)
- About one-half of alkalinity required for nitrification is produced in anoxic zone

# WWTP Changes to Achieve Nitrification-Denitrification

- Modify rectangular aeration basin with baffles to provide anoxic and aerobic zones
- Modify oxidation ditch to provide anoxic and aerobic zones
- Modify oxidation ditch operation with on/off aeration cycles to achieve denitrification
- Modify SBR system to include anoxic and aerobic cycles
- Modify step-feed system to include alternating anoxic and aerobic zones anoxic and aerobic zones at referencesses

## **Conventional Activated Sludge**



# Add an Anoxic Zone using Baffle, Mixed Liquor Return, and Mixing



## **Before and After Effluent Quality**

#### **Effluent Quality:**

BOD<sub>5</sub> TSS Ammonia-N NO<sub>x</sub>-N Total N \*SVI

**Before** 5 - 25 mg/l 10 - 25 mg/l 1 - 5 mg/l8 - 15 mg/l 10 - 20 mg/l 125 - 225

#### <u>After</u>

- 5 15 mg/l
- 10 20 mg/l
- 1 2 mg/l
- 3 9 mg/l
- 5 12 mg/l
- 50 125

\* impacts on mixed liquor at one facility

### **Oxidation Ditch Before Modification**



### **Oxidation Ditch After Modification**



# Intermittent Aeration for N Removal in Oxidation Ditch

- Cycle time for on/off operation of aerators may vary
- Process control with DO and ORP monitoring
- When aerator is off, must provide mixing
- During off period, oxidation ditch becomes anoxic reactor, and nitrate is consumed as bacteria degrade BOD
- ORP data are used to terminate off cycle and start aeration

# Change in ORP and DO in On/Off Operation



## Factors Affecting On/Off Operation

- Oxidation ditch HRT
- Influent flow rate
- TKN and BOD concentrations
- Number of on/off cycles per day
- Ditch MLSS concentration

## Nitrogen Removal in SBRs

- Use anoxic and aerobic cycles to effectively remove nitrogen
- Cycles are:
  - Fill (anoxic)
  - React (aerobic/anoxic)
  - Settle
  - Decant

#### Nitrogen Removal in SBRs

**Expected Effluent Quality:** 

BOD<sub>5</sub> TSS Ammonia-N NO<sub>x</sub>-N Total N 5 - 15 mg/l 10 - 20 mg/l < 1 mg/l 3 - 10 mg/l 5 - 12 mg/l

#### **N** Removal in Step-Feed Process

